

# Extended edition: What is a spectrum hole and what does it take to recognize one?

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# Extended edition: What is a spectrum hole and what does it take to recognize one?

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## Abstract

“Spectrum holes” represent the potential opportunities for non-interfering (safe) use of spectrum and can be considered as multidimensional regions within frequency, time, and space. The core challenge for secondary radio systems is to be able to robustly sense when they are within such a spectrum hole. To allow a unified discussion of the core issues in spectrum sensing, the “Weighted Probability of Area Recovered (WPAR)” metric is introduced to measure the performance of a sensing strategy and the “Fear of Harmful Interference”  $F_{HI}$  metric is introduced to measure its safety. These new metrics explicitly consider the impact of asymmetric uncertainties (and misaligned incentives) in the system model. Furthermore, they allow a meaningful comparison of diverse approaches to spectrum sensing unlike the traditional triad of sensitivity, probability of false-alarm  $P_{FA}$ , and probability of missed detection  $P_{MD}$ . These new metrics are used to show that fading uncertainty forces the WPAR performance of single-radio sensing algorithms to be very low for small values of  $F_{HI}$ , even for ideal detectors. Cooperative sensing algorithms enable a much higher WPAR, but only if users are guaranteed to experience independent fading. Finally, in-the-field calibration for wideband (but uncertain) environment variables (e.g. interference and shadowing) can robustly guarantee safety (low  $F_{HI}$ ) even in the face of potentially correlated users without sacrificing WPAR.

## I. INTRODUCTION

Wireless systems deliver real value to their users, but require radio spectrum to operate. The use of a band of spectrum by one system in the vicinity of a second system’s receiver (tuned to the same band) will generally degrade the performance of that second system if the total interference exceeds a critical value.<sup>1</sup> Therefore, spectrum is in principle a potentially scarce resource. Indeed, across the planet, spectrum is regulated so that most bands are allocated exclusively to a particular service, often with only a single system licensed to use that band in any given location. It is generally illegal to transmit without an explicit license. It is the *fear* of harmful interference that drives this policy of prior restraint.

This approach has been largely successful in avoiding interference, but in practice it does so at the expense of overall utilization. *Most bands in most places are underused most of the time* [3]–[5]. A band of spectrum can be considered underused if it can accommodate secondary transmissions without harming the operation of the primary user of the band.<sup>2</sup> The region of

<sup>1</sup>The performance degradation with increased interference can be gradual in the case of analog systems or catastrophic in the case of digital systems. While the critical value of total interference is therefore relatively unambiguous for digital receivers, a subjective judgment of “minimally acceptable quality” is required for analog systems. In the literature, the critical value of total interference is called the “interference temperature limit” [1], [2]. The terminology itself is meant to suggest that interference can be considered to be like additional thermal noise.

<sup>2</sup>Using the language of interference temperature, underutilization is said to exist whenever the actual interference temperature at a location has not yet reached the specified interference temperature limit [1], [2]. However, it turns out that interference temperature alone is not enough to understand the concept of a spectrum hole [6]–[8].

space-time-frequency in which a particular secondary use is possible is called a ‘spectrum hole.’ Spectrum holes are defined and discussed further in Section II.

Upon reflection, spectrum holes are a natural consequence of the gap between the distinct scales at which regulation and use occur — *just as a vase can be filled with rocks and still have plenty of room for sand*. Spectrum regulatory agencies perform allocations that are valid for multiple years/decades and over spatial extents that are hundreds of miles across. This is despite the fact that useful spectrum use could occur even over a few milliseconds and in a manner that is localized around transmitter-receiver pairs only tens of meters apart.

Why then do not regulatory agencies simply adjust their regulatory granularity to deal with scales closer to those of actual use? If a *static* approach to spectrum access is assumed wherein devices and wireless systems are inherently tied to particular bands and the regulator acts by certifying devices and systems before they are put into service, then the regulatory granularity is lower-bounded by the natural lifespans of wireless systems and the mobility of the devices. The lifespan of a wireless system is governed by the business models for the service — the system has to operate for long enough to result in a positive return on the infrastructure investments. The lifetime might differ wildly from one application to another<sup>3</sup> — and thus by Moore’s law, the technical sophistication of wireless systems can and will differ greatly from each other. The freedom of innovation and movement for the users of one system translates into uncertainty for the operators of another. *The unknown is feared if it can affect you*. To reduce this fear of harmful interference, the interaction must be precluded by ensuring that different users are in different bands even after they have physically moved.

Yet the overall demand mix for different applications/services is almost certain to be different from one location to another, and so in a world of heterogeneous wireless services and static allocations, waste is seemingly unavoidable. This also precludes otherwise brilliant approaches (see e.g. [9], [10]) that design transmissions so that the interference at receivers is aligned roughly orthogonal to their desired signals. Such an approach is not practical for heterogeneous services because it requires the potentially interacting systems to jointly coordinate their transmissions.

Bridging this gap and filling in spectrum holes requires a *dynamic* approach to spectrum access. Wireless systems must determine where the holes exist and reconfigure to take advantage of these opportunities. Regulation shifts from the level of the allocations themselves to the level of dynamic allocation strategies. The goal of this paper is to give a unified perspective on finding spectrum holes without inducing an unacceptable fear of harmful interference. The subsequent use of these spectrum holes as well as the design/enforcement of the regulations are both outside the scope of this paper.

Cognitive radios have been proposed to be the next generation devices that can dynamically share underutilized spectrum [2], [11], [12]. Spectrum sensing has been identified as one of the key enablers for the success of cognitive radios [6], [13]. There has been a lot of work on designing sensing algorithms for cognitive radio systems. Table I gives a brief sampling of some representative single-user sensing techniques. The techniques given in Table I are by no means exhaustive. The reader is encouraged to look into the references within these references for more. In addition to single-user techniques, cooperative approaches have also been proposed. A brief survey of cooperative sensing approaches is given in Table III. However, spectrum

<sup>3</sup>Compare the longevity of analog television to the different cellular or Wireless Local Area Network (WLAN) standards that have come and gone within the same time period.

sensing is still very much an active area of research and so in this paper we *do not* aim to find the best possible sensing algorithm for identifying spectrum holes. Instead, the goal here is to understand the key concerns in sensing and how different approaches can be compared to each other.

We start by understanding the basic issues in identifying spectrum holes. To do so, it is easier to concentrate on two extreme cases. First consider primary transmitters like television towers that are always communicating to users in their service area. Some of the area around the primary transmitter can never be used (the red area in Figure 1(a)) while area further away (green area in Figure 1(a)) could always be used by secondary users. For bands with such primary users, recovering spectrum holes in *space* is the major concern. Contrast this to a system that transmits intermittently but serves the entire area of interest (see Figure 1(b)). For such a band, recovering spectrum holes in *time* is the major concern.

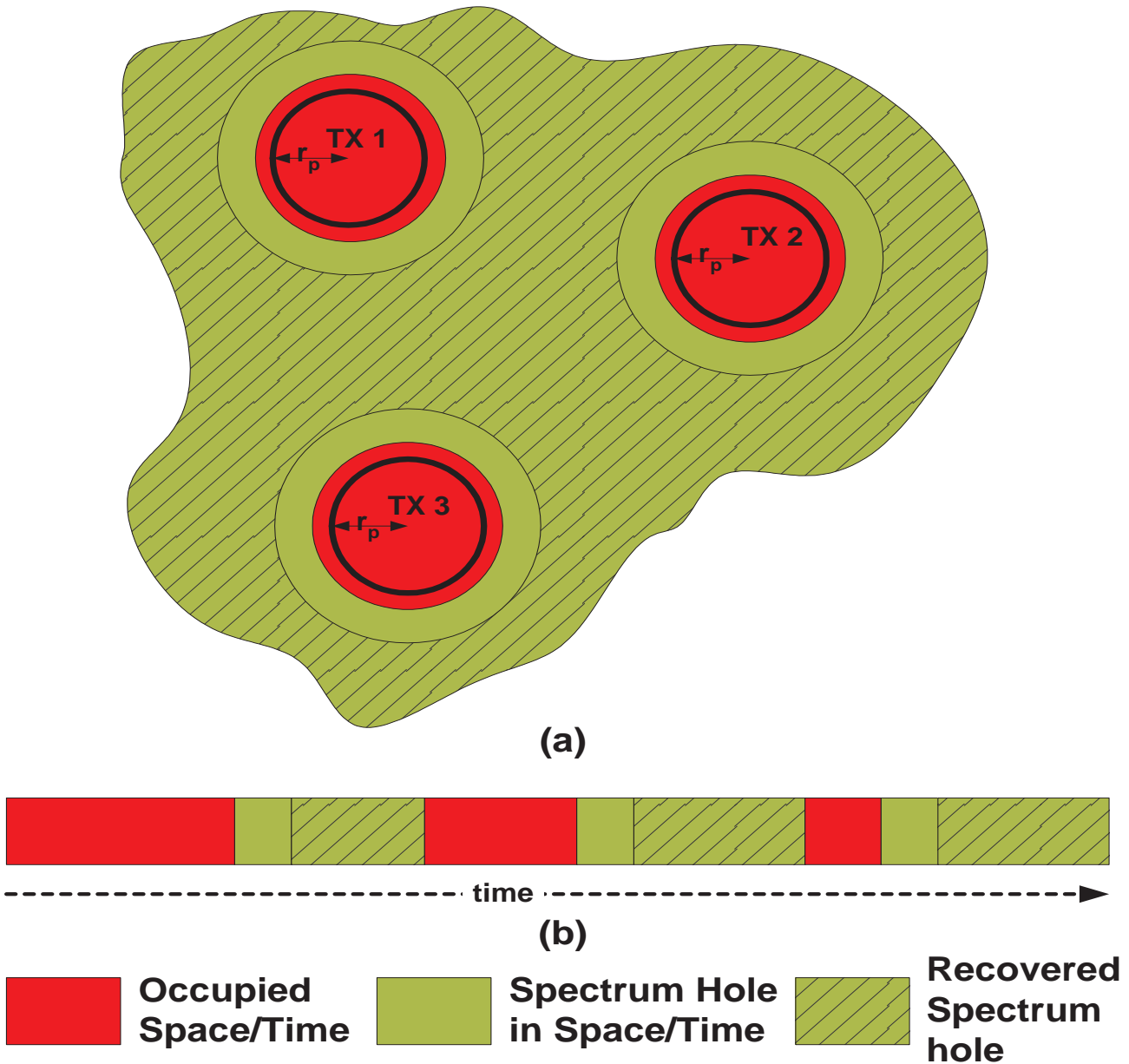


Fig. 1. (a) Spectrum holes in space. Area around each transmitter (shaded red) can not be used for secondary transmissions. However the shaded green area can be used all the time. (b) Spectrum holes in time. The secondary user cannot transmit while a primary transmission is on (shaded red). A secondary user can hope to reuse the off times of the primary user (shaded green).

| <i>Detection algorithm</i>               | <i>Description of algorithm</i>  | <i>What is modeled?</i>  | <i>To what gain?</i>              |
|--|--|--|-----------------------------------|
| Energy detection [14]–[16]               | Get empirical estimate of energy in a frequency band and compare against a detection threshold.  | Average power  | Baseline detector for comparison. |
| FFT for DTV pilot signal [17]–[19]       | Partial coherent detection using DTV pilot. Filter around pilot to reduce noise power. Use FFT as partial coherent detector for sinusoids. | Signal contains narrowband pilot tone  | Sensing time and robustness       |
| Run-time noise calibrated detection [20] | Noise is calibrated during run-time leading to robustness gains.   | Asymmetric use of degrees of freedom   | Robustness gains.                 |
| Cyclostationary detection [21]–[25]      | Spectral correlation function reveals peaks at multiples of the modulation rate/pilot frequency.   | Signal is modeled as wide-sense cyclostationary  | Robustness gains                  |
| Dual FPLL pilot sensing [26]             | Use two Digital PLLs which are preset to $\pm 30\text{kHz}$ around the pilot. Use time to converge as test statistic.                      | Signal contains narrowband pilot tone  | Simplicity of implementation      |
| Eigenvalue based detection [27], [28]    | Utilizes the fact that white noise is uncorrelated across samples/antennas while a band-limited external signal is correlated              | Band-limited primary signal and secondary radio has multiple receive antennas                | Sensing time gains                |
| Event-based detection [29], [30]         | The detector tries to detect arrival/departure of signals. This technique can be used for identifying time-domain holes.                   | Primary user ON/OFF durations are much shorter than the time between secondary user movement | Robustness gains                  |

TABLE I

COMPARISON OF REPRESENTATIVE SINGLE-USER SENSING ALGORITHMS FOR DTV DETECTION. THESE ALGORITHMS USE VARIOUS FACETS OF THE TRANSMITTED SIGNAL TO OBTAIN A BETTER DETECTION SENSITIVITY OVER SIMPLE ENERGY DETECTION.

Traditionally, the time-perspective has dominated the literature. The triad of sensitivity, probability of missed detection ( $P_{MD}$ ), and probability of false alarm ( $P_{FA}$ ) have been used to evaluate the performance of sensing algorithms [31]. The first two are connected to the level of protection for the primary users while the last is connected to the performance of the secondary user. Meanwhile, the time required to sense provided a measure of the overhead imposed by the sensing strategy. The tradeoff between these four metrics provided the sensing-layer interface to the overall tradeoff between the level of protection/safety offered to the primary user and the secondary system performance, but there is not a one-to-one mapping. Secondary system performance is naturally measured using expected throughput, but this makes sense only in the context of a complete system model. Thus, the design problem can be stated as a cross-layer optimization problem of maximizing the data rate while ensuring that the weighted probability of missed detection (the proxy for primary user safety) is bounded [32], [33].

While the cross-layer optimization approach does allow the comparison of disparate sensing strategies, it does so only in the context of a complete system model. Conceptually, this is disturbing because it tightly couples the internals of sensing spectrum holes to the communication strategy used once the holes have been found. We believe that this indicates that the traditional metrics do not represent the right level of abstraction — to have a unified perspective, we need uniform metrics that can compare sensing algorithms (both single-user and cooperative approaches) at the sensing layer itself. The advantage of this approach is that it gives us the freedom to design sensing algorithms without explicitly worrying about higher-layer considerations.<sup>4</sup> Moreover, these metrics must also allow us to incorporate modeling uncertainties, which can significantly

<sup>4</sup>This is also desirable from a regulatory perspective. Requiring re-certification of a complete system each time anything changed would be a tremendous obstacle to innovation. The main goal of regulation is to preserve safety — and this is determined by the operation of the sensing-layer.

impact the sensing performance.

The need to incorporate uncertainties can easily be seen in the time-domain. For example, exploiting time-domain spectrum holes in the context of Bluetooth and Wireless LAN coexistence has been considered in [34]. The key to exploiting such opportunities in time is the secondary user's ability to predict the OFF times of the primary users [35], [36]. While these results have established that dynamic spectrum access has the potential to dramatically increase the amount of spectrum available for use, a drawback is that these approaches depend on the detailed model for the primary user's transmissions. However, real-world uncertainties make it impossible to model real-world transmissions precisely (see [37] for an example from computer networking) and deviations from the assumed model can severely affect the performance of these algorithms leading to interference to the primary system<sup>5</sup>.

The essence of the discussion above is the need for having unifying sensing metrics that capture the right level of abstraction while allowing the incorporation of the relevant modeling uncertainties. It is not too hard to intuit the form of these metrics for the problem of identifying time-domain holes. To get a unified perspective on spectrum sensing, this paper develops the corresponding metrics for the problem of recovering spectrum holes in space. This problem is non-trivial and is not well understood in the previous literature. A brief comparison of the time-domain and the spatial-domain is given in Table II. The main contributions of this paper are:

- The issue of uncertainty and its modeling is discussed in detail. In particular, the asymmetric nature of the incentives regarding uncertainty-modeling is considered to be at the heart of the dynamic spectrum-recovery problem rather than being merely an annoying complication.
- An explicit approach is given to quantify the Fear of Harmful Interference ( $F_{HI}$ ) by maximizing the probability of interference under the worst-case environment consistent with the uncertainty model.
- A unified metric, Weighted Probability of Area Recovered (WPAR), is given to measure overall sensing performance. This allows for a simple analysis that decouples different primary users.
- Cooperative approaches are discussed not just under ideal models, but also with the uncertainty that is the unavoidable companion to freedom.
- In-the-field calibration is introduced as a mechanism to reduce environmental uncertainties that have a wider bandwidth than the primary user. Examples of such uncertainties are interference and shadowing.

The rest of the paper is organized as follows: After Section II formally defines a spectrum hole, Section III discusses the relevant metrics to quantify safety (non-interference) and the area recovered. Section IV illustrates the use of the metrics by considering a single-radio approach to finding spectrum holes and reveals the fundamental limitations of the IEEE 802.22 approach to evaluating detectors [42]. The example of the radiometer is used to connect these metrics to earlier perspectives as well as to show how to incorporate the impact of finite sensing times and uncertainty in the fading model. Section V discusses both the potential gains of cooperative detection and their sensitivity to shadowing-correlation uncertainty. Section VI discusses

<sup>5</sup>This is analogous to open-loop control in stochastic systems [38], [39]. Systems with open-loop control rely heavily on precise and accurate modeling. In contrast, closed-loop control systems can be much more robust to modeling uncertainties. One possible approach to resolve this uncertainty in the spectrum-sharing context is feedback from the primary system. Such feedback can significantly help in robustly exploiting opportunities in the time domain. Opt-in spectrum markets are an extreme case of explicit feedback from primary users [40], but other forms of implicit feedback are also possible. For example, [41] proposes a spectrum-sharing architecture in which the secondary user eavesdrops on a packetized primary user's automatic repeat request (ARQ) messages to stay within the interference budget of the primary users.

the use of measurements in nearby bands (eg. satellite bands) to enable assisted detection and points to a way to overcome the uncertainty regarding shadowing correlation. Section VII revisits the lessons of this paper and concludes with pointers to future work.

## II. DEFINING A SPECTRUM HOLE IN SPACE

In time the definition of a spectrum hole is easy to understand — it is the period of time that the primary is not transmitting. A spectrum hole in frequency is a little more nuanced. If a secondary user finds a frequency band empty (no primary user present in that band), its transmissions can still interfere with primary receivers operating in adjacent frequency bands (due to imperfect filters and analog front-ends). Hence, a spectrum hole in frequency is technically defined as a frequency band in which a secondary can transmit without interfering with any primary users (across all frequencies). For simplicity, we suppress this subtle distinction in this paper and consider a spectrum hole in frequency to be a contiguous band of frequencies which is not used locally by any primary user. For further simplicity, we will consider only one such specified frequency band at a time.

**Definition 1:** Consider a perfect magical detector that tells us whether it is safe to use a particular secondary system at a given point in space-time or not. Denote the output of this detector (safe-to-transmit region) by  $D^* \subset \mathbb{R}^3$  where two of the dimensions represent space and the third represents time. A *spectrum hole* in space-time is defined as an indicator function  $\mathbf{1}_{D^*} : \mathbb{R}^3 \rightarrow \{0, 1\}$  defined as

$$\mathbf{1}_{D^*}(\mathbf{x}) = \begin{cases} 1 & \text{if } \mathbf{x} \in D^*, \\ 0 & \text{if } \mathbf{x} \in \mathbb{R}^3 \setminus D^*. \end{cases}$$

For further simplicity, we focus on a frequency band which is licensed to a single primary service. The primary transmitters dealing with this particular band are assumed to be distributed over a large geographic area with non-overlapping service areas. For example, consider television bands where primary transmitters are stationary and have long-lived transmissions. A television station’s transmitter is mounted on a high tower ( $\approx 500$  m) and serves a large radius ( $\approx 50$  km). Further away, the signal from the tower is very weak and a secondary user at such a location can transmit without causing interference. Our attention will mostly be focused on a single one of those towers and the area around it.

Figure 2 shows a primary transmitter and a single primary receiver. In the absence of interference, a receiver within the blue circle (Figure 2a) with radius  $r_{dec}$  would be able to decode a signal from the transmitter, while a receiver outside the circle would not. To tolerate any secondary users, the primary receiver needs to accept some additional interference. The green circle represents the protected radius (denoted  $r_p$ ) where decodability is guaranteed to primary receivers. Primary receivers between the two circles may not be able to get service once secondary systems come on, but this is considered to be an acceptable loss of primary user QoS.<sup>6</sup> Call these “sacrificial zones.” The time-dimension equivalent of  $r_{dec} - r_p$  is the short sacrificial time-segment at the beginning of a primary transmission during which secondary users are permitted to cause interference.<sup>7</sup>

<sup>6</sup>This can be viewed as either the loss of service to certain customers of the primary system or as an additional cost of transmit power that must be spent by the primary user to maintain service to all the same customers.

<sup>7</sup>Like its spatial equivalent, this can be viewed as either a loss of QoS for the primary user in the sense of a dropped frame or as requiring the primary user to lengthen its synchronization preamble before commencing data transmission. Without this provision, a secondary user can never transmit due to the fear of primary user reappearance during the secondary transmission.



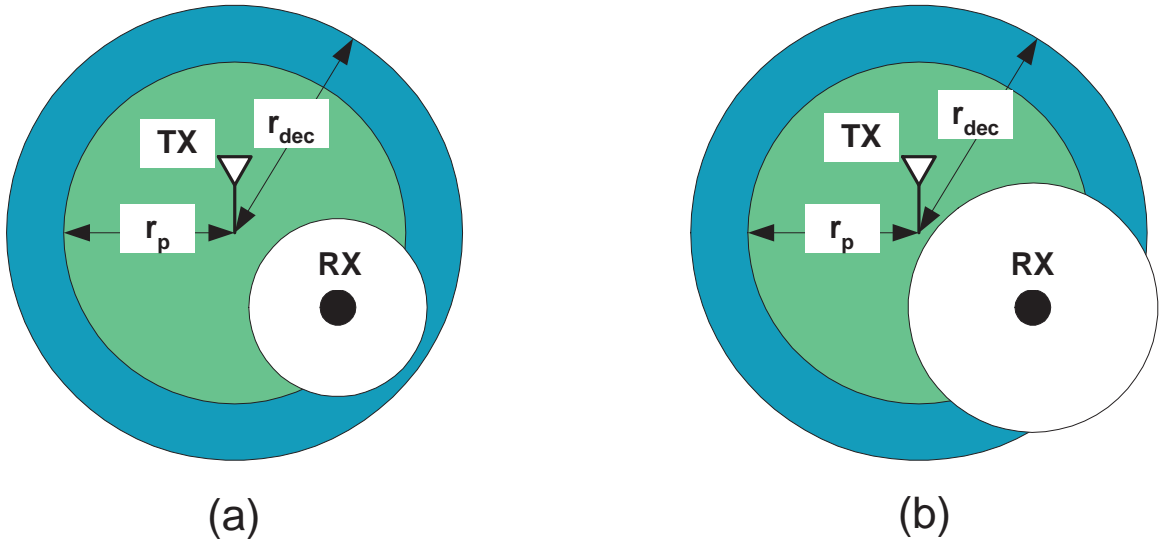


Fig. 2. Weaker secondary users can transmit closer to the protected primary receivers, whereas louder secondary users can only transmit far from the protected primary receivers.

Around each protected primary receiver, a no-talk region exists where a secondary user cannot safely transmit. However, this depends on the nature of the secondary transmission. If it has low transmit power, (Figure 2a) then the no-talk zones around each receiver can be small. If it has high transmit power, (Figure 2b) the radius of the no-talk zones will become much larger. There are two ways to interpret this effect. One approach is to consider the transmit power of the secondary user as its footprint and think of the secondary user as a finite-sized ball (of radius  $(r_n - r_p)$ ). In this approach, the question becomes whether the ball fits into the hole. For simplicity, a second approach is followed here: the secondary user is considered to be a point and the spectrum hole itself is considered to not include those points at which a secondary user would not safely fit.<sup>8</sup>

The overall no-talk area is thus the union of the no-talk regions of all primary receivers. The spectrum hole is the complement of this union. To recover this area, the secondary system must know the locations of all primary receivers (see Figure 3(a)). Since a primary user may know this information, such complete area recovery might be possible with explicit primary participation. In addition, secondary users themselves may be able to determine the locations of receivers for particular TV channels by sensing the TV receivers themselves [44].

However, just because a secondary transmitter *can* safely transmit in a particular location on a particular band does not imply that it should want to do so. After all, close to a functioning primary receiver there will usually be a lot of interference from the primary signal itself. It has been proposed that the secondary transmitter may be able to decode the TV signal and use dirty-paper-coding techniques (DPC) and simultaneously boost the primary signal in the direction of interference [45], [46]. However, it has also been shown that this approach is not robust since simple phase uncertainty can significantly lower the performance of such schemes [47]. Other forms of partial information like knowledge of the primary user's codebook are also not useful unless the secondary receiver can actually decode the primary signal and use multiuser detection. Otherwise,

<sup>8</sup>For simplicity, this discussion assumes a single simultaneous secondary transmission. In practice, the secondary system is likely to contain many transmitters operating simultaneously over a distributed area. Such systems can have their user footprints considered in terms of their power density as shown in [7], [8]. However, the analysis in [43] shows that the first interpretation becomes problematic when we really try to scale to secondary users with very different footprints.

it has been shown that the secondary system is forced to treat the primary transmission as noise [48]. Since even marginally decodable primary signals tend to be far louder than the background noise, this suggests that knowledge of the locations of the primary receivers is not that useful in practice.

Consequently, this paper focuses on recovering the region outside the global no-talk zone ( $r_n$ ) as shown in Figure 3(b). This is the intersection of the spectrum holes corresponding to all possible locations for protected primary receivers. In this picture, knowledge of the relative positions of the primary transmitters and the potential secondary user is key.

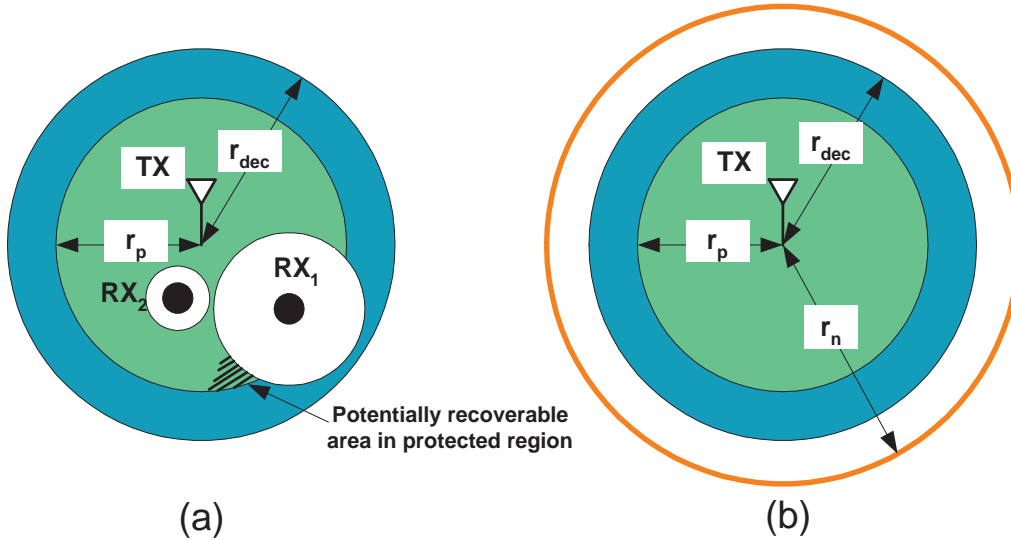


Fig. 3. (a) Area within the protected region can be recovered if the positions of the primary receivers can be determined. (b) Global no-talk area defined assuming the primary receivers can be anywhere within the protected region

### III. METRICS AND MODELS

The main task of the secondary system is to determine its relative position with respect to the primary transmitters and to start transmission only if it is reasonably sure that it will not interfere with any of the potential primary receivers. An ideal solution is to require the primary user to register all of its transmitters' positions and for the secondary system to possess the ability to calculate its own position as well as communicate with the registry that records primary user positions.

While the above works for purely spatial spectrum holes, it does not scale well to spectrum holes that span both space and time. It also involves a lot of overhead. Therefore, we must consider different approaches to detecting spectrum holes and have metrics that can be used to compare their performance.

#### A. Signal to Noise Ratio (SNR) as a proxy for distance

A natural approach is for the secondary user to estimate the strength of the primary signal as a proxy for the distance from the primary transmitter. The problem then becomes: at what level must the secondary user detect the primary system to be reasonably sure that it is outside the no-talk radius? If  $p_t$  (in dBm) is the transmit power of the primary user and  $\alpha$  is the

attenuation exponent<sup>9</sup>, then the secondary user can transmit if the received power from the primary user at the secondary user is less than  $p_t - 10 \log_{10}(r_n^\alpha)$  i.e.

$$P \underset{\text{use}}{\overset{\text{do not use}}{\leq}} p_t - 10 \log_{10}(r_n^\alpha), \quad (1)$$

where  $P$  (in dBm) is the received primary power at the secondary radio. In general,  $P$  is a random variable and its realization can be computed by taking the log of the empirical average of the square of the received primary signal (See Section IV-B).

We interpret Equation (1) as follows: the secondary radio declares the band to be free only if the received power is strictly less than the threshold, in this case  $p_t - 10 \log_{10}(r_n^\alpha)$ . If the received power is greater than or equal to  $p_t - 10 \log_{10}(r_n^\alpha)$ , the secondary radio declares the band to be occupied. We use this same interpretation for all the threshold based detection rules in this paper.

The detection rule in (1) assumes that a system can deterministically determine its relative position given only the received signal strength and thereby recover all the area beyond the no-talk radius. In reality, the primary signal may experience severe multipath and shadowing which results in a low received power. Seeing a low power signal, the secondary user may decide that it is outside the no-talk radius while in fact it is inside. Hence, a system must somehow budget for such fading. One possible approach is to introduce a design parameter,  $\Delta$  (in dB), which is the combined budget for possible fading and shadowing losses. Then, the rule in (1) becomes:

$$P \underset{\text{use}}{\overset{\text{do not use}}{\leq}} p_t - (10 \log_{10} r_n^\alpha + \Delta). \quad (2)$$

In (2), the parameter  $\Delta$  is a constant serving the role of a safety factor. Its value is determined by the desired operating point of the system, and it is fixed at design time. The value of  $\Delta$  impacts the secondary user's ability to guarantee non-interference to the primary user as well as to recover area for its own operation. If  $\Delta$  is large then the secondary user acts conservatively and only declares an area usable when the primary signal is very weak. In normal circumstances such weak signals occur very far from the TV transmitter and the secondary user must forfeit a lot of the area around the primary transmitter (see Figure 4) but it is able to ensure non-interference to the primary user. If  $\Delta$  is small, there is a chance that the secondary user will not even sense moderately faded primary signals. The secondary user will then be interfering with the primary user more often but will forfeit a smaller area (see Figure 4). This tradeoff needs to be captured in the appropriate metrics.

## B. Traditional sensing metrics

We briefly review the traditional triad of sensing metrics (sensitivity,  $P_{FA}$ , and  $P_{MD}$ ) and motivate the need for system-level metrics for the problem of identifying spatial spectrum holes.

Any sensing algorithm can be thought of as a system (black box) with inputs, outputs and control knobs. The input to the system is the received signal, and the output is the decision whether the band is usable or not. The control knobs are design parameters like detector threshold, sensing time, etc. Traditionally, the performance of such a system is characterized by its

<sup>9</sup>A commonly agreed propagation model for DTV signals transmitted from TV towers is given in [49]. The pathloss function described by this model (see Figure 1 in [50]) can be approximated by a continuous piecewise polynomial function. Explicitly, for all the figures in the paper we use an exponent of  $\alpha = 3$  for distances below 1 km, an exponent of  $\alpha = 2.7$  till 30 km, an exponent of  $\alpha = 7.65$  till 100 km, and an exponent of  $\alpha = 8.38$  from there on. However, to keep the expressions in the text simple, we use a single polynomial with exponent  $\alpha$  for the pathloss function.

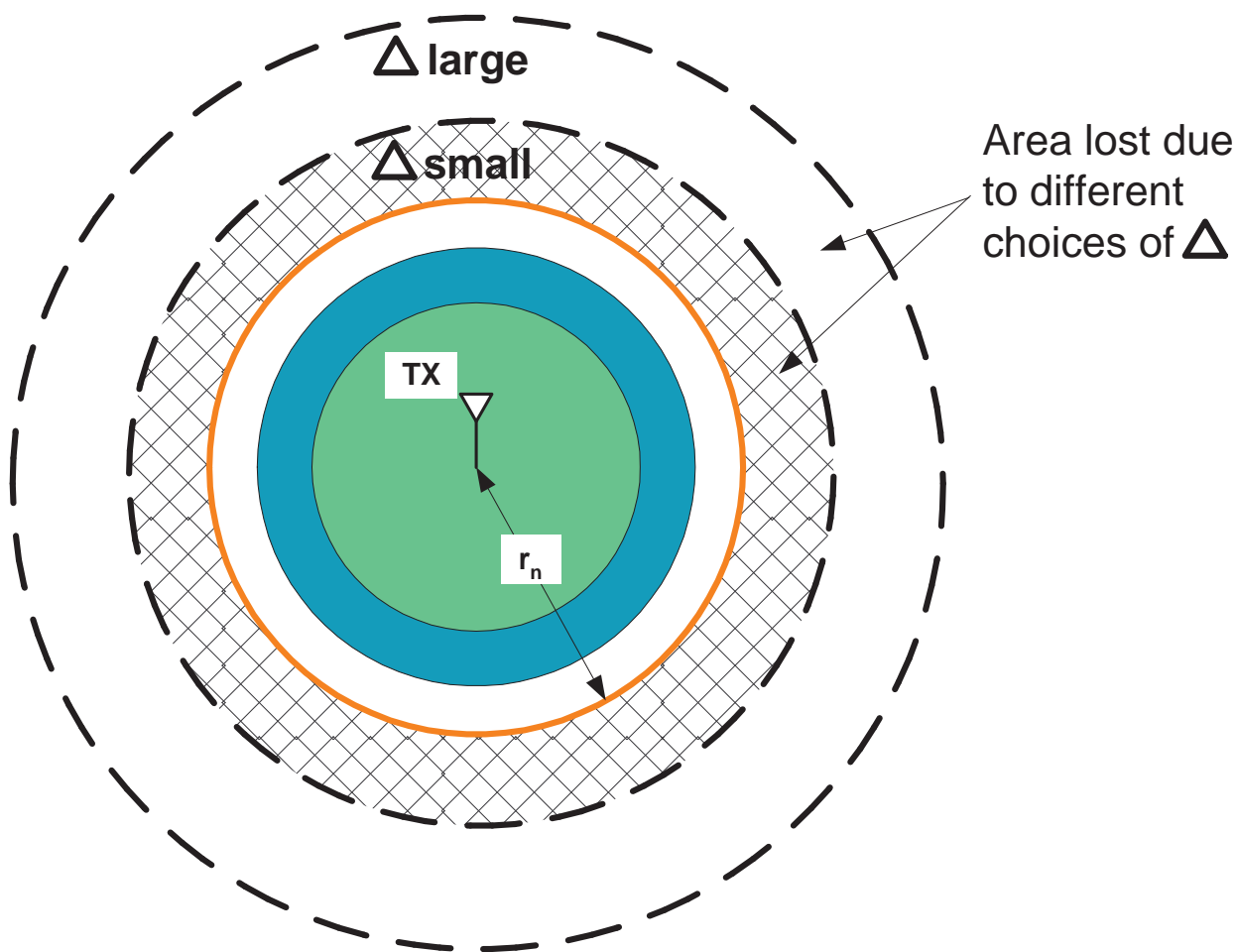


Fig. 4. If the budget for multipath and shadowing is small ( $\Delta$  small), then the secondary user does not forfeit much area beyond the true no-talk zone. If the budget for multipath and shadowing is large ( $\Delta$  large), then the secondary user forfeits a lot of area outside the no-talk zone.

*Receiver Operating Characteristic (ROC) curve.* The ROC of a detector is a curve that plots the  $P_{MD}$  as a function of the  $P_{FA}$  for a fixed sensing time, and fixed operating  $SNR$  [51]. An alternate performance metric for a detector is its *sensitivity*. The sensitivity of a detector is the lowest value of the operating  $SNR$  for which the detector satisfies a given target  $P_{FA}$  and  $P_{MD}$ .

The overhead for a detector is traditionally measured by the sensing time required to achieve a target  $P_{FA}$ ,  $P_{MD}$  at a given  $SNR$ . This is called the *sample complexity* of the detector. The sample complexity and sensitivity are tightly coupled — if we want to improve the sensitivity of the detector, we must increase the sample complexity and hence incur a larger sensing overhead.

An important functional requirement for detectors operating at low  $SNRs$  is *robustness* to uncertainties in the system. Uncertainties can be broadly divided into two classes — device-level uncertainties (like uncertainty in the noise power) and system-level uncertainties (like uncertainty in the shadowing distribution). It was shown in [16] that the traditional metrics can be suitably modified to characterize detector robustness to device-level uncertainties. This was done by considering worst-case  $P_{FA}$ ,  $P_{MD}$  over the set of uncertain distributions. Furthermore, it was shown that detectors have fundamental  $SNR$  thresholds called *SNR walls* below which detection was impossible even if the sensing time is increased to infinity. This showed that

| <i>Quantity of interest</i>          | <i>Time domain</i>  | <i>Spatial domain</i>   |
|--------------------------------------|---|---|
| Interference margin                  | Permissible duration of secondary interference at the start of primary user's ON period | Marginal area relinquished by primary users to allow secondary operation        |
| Modeling uncertainty                 | Distributional uncertainty in the primary users' ON/OFF periods                         | Distributional uncertainty in the primary signal's fading/shadowing             |
| Scenario for computing safety metric | Worst-case overlap between primary's and secondary's transmissions                      | Worst-case placement of secondary users within the no-talk region               |
| Performance metric                   | Fraction of primary user's OFF period recovered for secondary transmission              | Area outside the primary's no-talk region recovered for secondary transmissions |
| Overhead                             | Sensing time  | Area outside the no-talk region that cannot be recovered                        |

TABLE II  
CORRESPONDENCES BETWEEN THE QUANTITIES OF INTEREST IN THE TIME AND SPATIAL DOMAINS.

under device-level uncertainties, we must consider both sensitivity and the detector's  $SNR$  wall as a measure of performance.

Now, the remaining question is: how do we deal with system-level uncertainties? The dominant current approach to deal with system-level uncertainties like uncertainty in shadowing is to incorporate them in the specifications for the system. For instance, to account for possible deep fades, the 802.22 working group specifications require detectors to have a sensitivity of  $-116$  dBm ( $-20$  dB  $SNR$ ) [42]. This corresponds to a safety margin of roughly  $\Delta = 20$  dB [14].

There are two fundamental problems with this approach. First, this approach is very conservative and leads to severe overheads ( $20$  dB  $\approx 110$  km). In most situations detectors do not face such severe fading and hence they are forced to not use the band even though they are well outside the no-talk radius. Secondly, this approach of specifying a sensitivity requirement is not compatible with cooperative sensing approaches. It is clearly hard even to define what sensitivity means for a whole group of radios [52]. What if one of them is faded and another is not?

### C. New system-level metrics

In the previous section we showed why the traditional sensing metrics fail to capture the right level of abstraction between the sensing and communication.

In Table II, we list the quantities/modeling philosophy that we want to capture with appropriate metrics. For the problem of recovering time-domain holes these quantities are well understood (listed in the second column of Table II). The analogous quantities in the spatial domain are listed in the third column of Table II.

We now give two new system-level metrics — safety to the primary user and sensing overhead given by the loss in area. The metrics have been defined to capture the essence of the discussion in Table II.

1) *Safety*: The first idea for a safety metric is to just calculate the probability of interference. However, this is a metric that is open to serious abuse. A secondary system might do no sensing and just assume that its users will be uniformly placed in a large area (much larger than the footprint of the TV station). Hence the probability of a user landing within the no-talk area is very small and the secondary system can claim compliance with a target probability of interference of 1%.

Such a metric for safety is essentially no better than the secondary system telling the primary user “trust me, my users are not going to be close enough to interfere with you.” The primary user has no reason to trust the *a priori* user-deployment

model of the secondary system once the secondary products are in the marketplace. There is an asymmetry here: the secondary operator might very well have a uniform-area business model in mind, but the primary user fears that the secondary operator will end up deploying the system close to the primary’s receivers since that is where the people are. A metric that accurately captures the primary’s fear of harmful interference must somehow assume the worst-case deployment of secondary users.

Similarly, there is no reason to completely trust the fading model. A detector could end up operating in line-of-sight environments or it could be deeply shadowed. For example, the secondary operator may propose roof-top static installations (with very little shadowing) of its access devices thinking that people will be using it to get Internet access in single-family homes. However, people living in apartment buildings might also start buying the devices. Some users might notice that system performance improves if they bring their devices indoors (becoming shadowed from primary transmissions). A new multiplayer video game might even arise that encourages people to use the device inside their minivans while driving around town. The primary user will not trust the secondary operator to alienate its own paying customers and it is hard to perfectly anticipate the environment of the future.

The following definition captures these model uncertainties.

**Definition 2:** Assume that the secondary user runs a spectrum-sensing algorithm that outputs a binary decision  $D$  about the state of the primary band: 1-used/0-unused. The *probability of potential interference*  $\mathcal{P}_{F_r}(D = 0|r_{actual} = r)$  at radius  $r \leq r_n$  is the probability that a secondary user is within the no-talk region and declares that the band is “unused”<sup>10</sup>. Here  $F_r$  is the probability distribution of the combined multipath and shadowing-induced fading at a distance  $r$  from the primary transmitter.

The exact value of this probability depends on the assumed model for shadowing and multipath. The primary users (and regulators) only trust that the true distribution is within the set  $\mathbb{F}_r$ . Hence the *Fear of Harmful Interference* ( $F_{HI}$ ) is defined as:

$$F_{HI} = \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r} \mathcal{P}_{F_r}(D = 0|r_{actual} = r). \quad (3)$$

The outer supremum reflects the uncertainty in secondary user deployments and the inner supremum reflects the uncertainty in the distribution of the fading. Explicit models for these uncertain distributions are discussed in Section III-D.

There is an analogous safety metric for spectrum holes in time where the goal is to reuse the primary user’s OFF time while avoiding harmful interference in ON times. In addition to the fading uncertainty, the distribution of the inter-transmission times of the primary transmitters must also be viewed as uncertain (see e.g. [37]) to preserve the freedom of action of the primary system’s users. In addition, the relative starting time of the potential secondary transmissions is also viewed as uncertain just as the secondary position in space is considered uncertain.

2) *Performance:* Next we consider a metric to deal with the secondary user’s performance — its ability to identify spectrum opportunities. If there were only a single primary transmitter, every radial distance  $r > r_n$  would be spectrum opportunity. For any detection algorithm, there is a probability associated with identifying such an opportunity, called the probability of finding the hole  $P_{FH}$ :

$$P_{FH}(r) = \mathcal{P}_{F_r}(D = 0|r_{actual} = r), \quad r > r_n. \quad (4)$$

<sup>10</sup>This does not necessarily mean that a secondary radio will actually transmit and cause interference.

In reality, secondary users might also be uncertain about the shadowing and fading distributions. In this case the secondary users can compute performance assuming the worst-case distribution in their uncertainty set. This uncertainty set is typically much smaller than the uncertainty set used in (3) to compute the safety performance to the primary user. This is because the primary user does not trust the secondary users' deployment model and hence assumes a larger uncertainty set. On the other hand the secondary users know their deployment model accurately as there is no incentive for the secondary users to lie to themselves. So, they can work with a much smaller uncertainty set to compute performance. For simplicity, we just shrink the uncertainty set to a single point and assume complete knowledge of the combined shadowing and fading distribution,  $F_r$ .

The goal is to combine the probabilities  $P_{FH}(r)$  into a single performance metric that allows a comparison among different sensing algorithms. One choice is the underlying utility of the secondary system, like the total throughput or profit. However, such holistic utility functions are intertwined with the system architecture and business models along with assumptions regarding the placement of all the primary transmitters and the population distribution of potential customers. It is useful to find an approximate utility function that decouples the evaluation of the sensing approach from all of these other concerns.

We make the reasonable assumption that secondary utility will increase whenever additional area is recovered by the sensing algorithm. Since we would like to decouple the sensing metric from the detailed model for primary deployments, it is useful to be able to state it in terms of a single primary transmitter. The difficulty is that if there is only a single primary transmitter, the total area of the spectrum hole is infinite. We propose a discounted-area approach analogous to the present-value of consumer utility proposed by [53].

**Definition 3:** The *Weighted Probability of Area Recovered* (WPAR) metric is

$$WPAR = \int_{r_n}^{\infty} P_{FH}(r)w(r) r dr, \quad (5)$$

where  $w(r)$  is a weighting function that satisfies  $\int_{r_n}^{\infty} w(r) r dr = 1$ .

The numerical results in this paper have been computed using an exponential weighting function,  $w(r) = A \exp(-\kappa r)$ . While similar results can be obtained for any other weighting function, the exponential weighting is not unreasonable for the following reasons.

- Since TV towers are often located around areas of high population density, areas around the no-talk region are more valuable in terms of deploying a secondary system than areas far away. This can be viewed as a spatial analogy to “banker’s discounting” in which money in the future is worth progressively less in present units. By Sutton’s law<sup>11</sup>, the economic value of an area is proportional to the number of potential customers there. Population densities are often modeled as decaying exponentially as one moves away from the central business district [55].
- As we move away from any specific tower, there is a chance that we may enter the no-talk zone for another primary tower transmitting on the same frequency. This can be viewed as a spatial analogy to “drug-dealer’s discounting” in which money in the future is worth less than money in the present because it is uncertain whether the drug dealer will survive into the future because of the arrival of the police or a rival gang [56].

<sup>11</sup>When asked why he robbed banks, the famous bank robber Willie Sutton is believed to have said “because that is where the money is” and so this general principle has been named after him [54].



Fig. 5. Location of transmitters for Channel 30 (566-572MHz) plotted using Google Maps.

Figure 5 shows the locations of TV transmitters for Channel 30 all around the United States [57]. In keeping with the current rural deployment assumptions of IEEE 802.22, we just consider “drug-dealer’s discounting” here and this sets the value of  $\kappa = 2 \times 10^{-5}$  for the paper, given the other parameters that are commonly used for digital television signals: primary transmit power  $p_t = 90$  dBm, no-talk radius<sup>12</sup>  $r_n = 150.3$  km, and a piecewise polynomial propagation model fitted to match Figure 1 in [50].

When dealing with intermittent primary users (i.e. trying to recover holes in time), the goal is to reuse the OFF time while minimizing the sensing time. To understand the relative burden of the sensing time, we need to appropriately weigh recovered opportunities in time. “Drug-dealer’s discounting” is appropriate since potential opportunities in the future may never materialize because there is a chance of the primary user re-appearing before then. Thus, there is a Weighted Probability of Time Recovered (WPTR) metric that is analogous to the WPAR metric proposed in this section.

<sup>12</sup>This corresponds to WRAN basestations in 802.22. Using 36 dBm for secondary transmitters gives the 150.3 km radius [50].



#### D. Models for fading uncertainty

The received primary signal strength  $P$  (in dBm) can be modeled as  $P = p_t - (l(r) + S + M)$ , where  $p_t$  is the power of the transmitted signal,  $l(r)$  is the loss in power due to attenuation at a distance  $r$  from the primary transmitter,  $S$  is the loss due to shadowing and  $M$  is the loss due to multipath fading. Unless specifically mentioned, we assume that all powers are measured in dB scale. We assume that  $l(r) = 10 \log_{10}(r^\alpha)$ , and  $\alpha$  is the true attenuation exponent.<sup>13</sup>

1) *Nominal model:* For convenience,  $S$  and  $M$  are assumed to be independent of  $r$  and to follow a nominal model for  $S+M$  that is Gaussian ( $S + M \sim \mathcal{N}(\mu_S, \sigma^2)$ ) on a dB scale. This implies that  $P \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(r) = p_t - (l(r) + \mu_S)$ . This is the distribution used to compute the WPAR as in (5). For the plots in this paper,  $\mu_S = 0$  dB and the standard deviation  $\sigma = 5.5$  dB were chosen to match standard assumptions in the IEEE 802.22 literature [50].

2) *Quantile models:* To compute  $F_{HI}$ , we cannot always use the nominal model for shadowing and multipath as it is important to model the fact that the primary user does not trust this model completely. Instead, it is possible that the primary user trusts only a quantized version (or a coarse histogram) of the fading distribution. Mathematically, we model this as a class of distributions ( $\mathbb{F}_r$ ) that satisfy given quantile constraints.

**Definition 4:** A *single-quantile model*  $\mathbb{F}_r$  is a set of distributions for the received signal power defined by a single number  $0 \leq \beta \leq 1$  and a function of  $r$  denoted  $\gamma(r, \beta)$ . A distribution  $F_r \in \mathbb{F}_r$  iff

$$\mathcal{P}_{F_r}(P < \gamma(r, \beta)) = \beta. \quad (6)$$

A *k-quantile model* is a set of distributions  $\mathbb{F}_r$  for the received signal power defined by a list of numbers ( $\beta_1 < \beta_2 < \dots < \beta_k$ ) and a corresponding list of functions ( $\gamma_1(r, \beta_1), \dots, \gamma_k(r, \beta_k)$ ). A distribution  $F_r \in \mathbb{F}_r$  iff  $\forall i \leq k$

$$\mathcal{P}_{F_r}(P < \gamma_i(r, \beta_i)) = \beta_i. \quad (7)$$

For consistency, the quantiles are chosen so that the nominal Gaussian  $\mathcal{N}(\mu(r), \sigma^2)$  is always one of the possible distributions for  $P$ .

$$\gamma(r, \beta) = \mathcal{Q}^{-1}(1 - \beta)\sigma + \mu(r), \quad (8)$$

where  $\mathcal{Q}^{-1}(\cdot)$  is the inverse of the standard Gaussian tail probability function.

Figure 6 shows a picture of the distributions allowed under the quantile model (5 learned quantiles) defined in this section. The set of allowed Cumulative Distribution Functions (CDF's) for  $P$  under our quantile model is precisely the set of all possible non-decreasing curves sandwiched between the upper and lower bounds shown in Figure 6. The dashed (black) curve in the figure shows that nominal Gaussian CDF for  $P$ , and the quantile constraints can be thought of as samples of the nominal CDF (the triangle points (in red) in the figure).

<sup>13</sup>We could include an uncertainty model for the attenuation exponent and include this in the computation of  $F_{HI}$ . However, for simplicity we assume complete knowledge of the attenuation exponent in this paper.

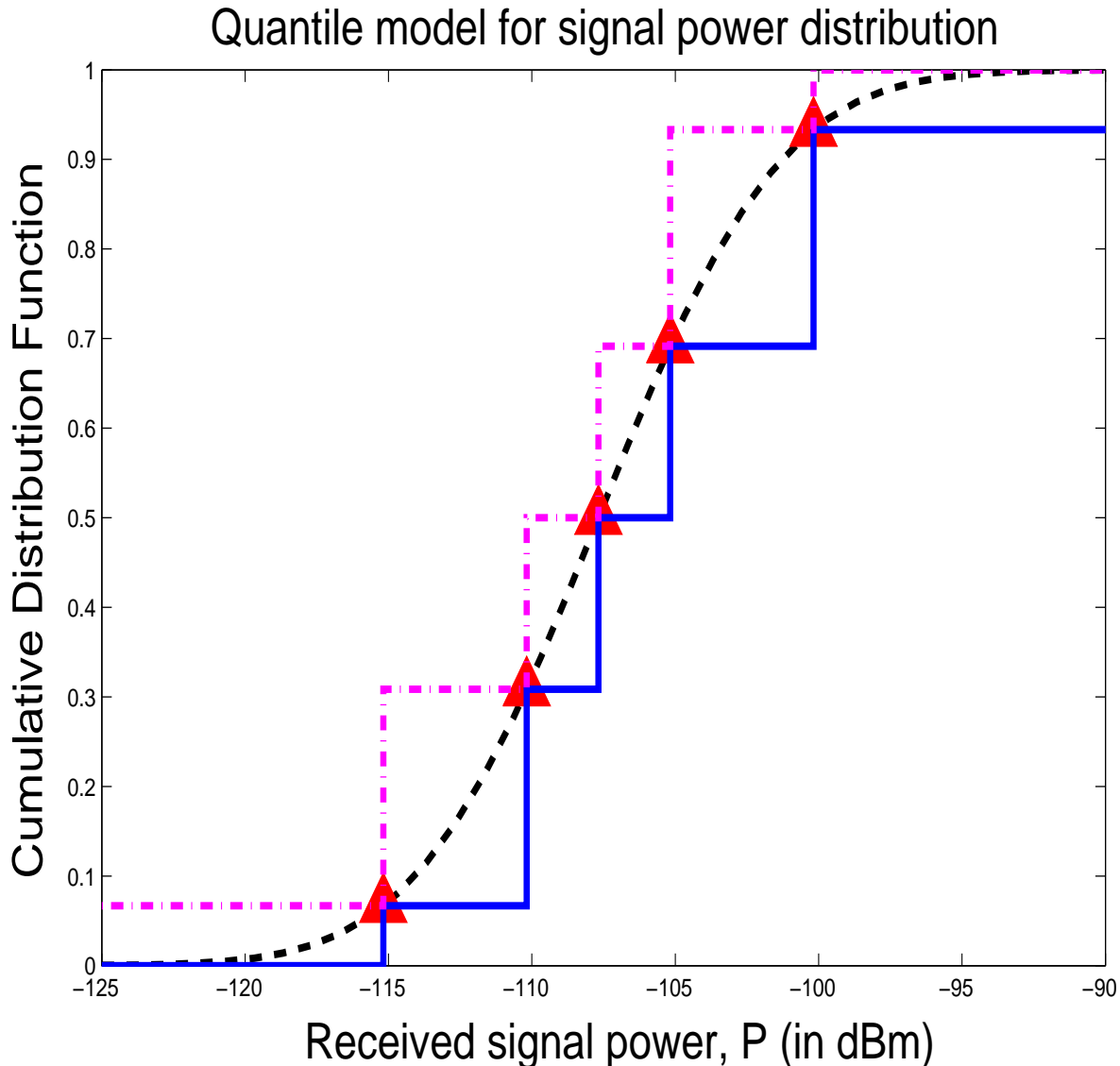


Fig. 6. The quantile model for the received signal power ( $P$ ) distribution. The dashed (black) curve is the nominal Gaussian CDF for  $P$ , and the triangle points (in red) show the quantile constraints on the CDF. The dashed-dotted (magenta) curve is the upper bound and the solid (blue) curve is the lower bound on the allowable CDF for  $P$ . The actual CDF can lie anywhere in between these two bounding functions.

#### IV. SINGLE RADIO SENSING PERFORMANCE

The tradeoff between  $F_{HI}$  and  $WPAR$  depends on the detector used by the secondary user. We start with a hypothetical detector that meets the current specification specified in the IEEE 802.22 process. The issue of finite sensing time is illustrated next through the example of a radiometer. A similar analysis could be carried out for any other detection algorithm and so the role of uncertain fading distributions is investigated using an ideal detector with an infinite sensing time.

##### A. Evaluating an ideal -116 dBm detector

The currently understood detector specifications in the IEEE 802.22 working group require any proposed sensing algorithm to be able to detect digital television signals at  $-116$  dBm to a probability of mis-detection  $P_{MD} \leq 0.1$  and probability of

false alarm  $P_{FA} \leq 0.1$  [42].<sup>14</sup> We now show that detectors based on such specifications lead to very poor area recovery and also do not guarantee safety beyond the 0.1 level without additional unspoken assumptions.

In the rest of the paper we assume that the received signal is sampled and hence we work in discrete time for simplicity. We assume a generic detection algorithm that computes a test statistic  $T(\mathbf{Y})$  as a function of the received signal samples  $\mathbf{Y} = (Y[1], Y[2], \dots, Y[N])$  and compares it to a threshold to decide whether the band is free to use or not, i.e.,

$$T(\mathbf{Y}) \underset{D=0}{\overset{D=1}{\gtrless}} \lambda.$$

Let  $P$  (in dBm) denote the average power of the received signal samples.  $P$  is a random variable whose distribution depends on the shadowing and fading distributions. Define the probability of mis-detection and probability of false-alarm to be

$$\begin{aligned} P_{MD}(p) &:= \mathcal{P}(T(\mathbf{Y}) < \lambda | P = p), \\ P_{FA} &:= \mathcal{P}(T(\mathbf{Y}) \geq \lambda | P = -\infty). \end{aligned} \quad (9)$$

Note that the probability of mis-detection is a function of the received signal power, where as the probability of false-alarm is a single number. For most reasonable detection algorithms  $P_{MD}(p)$  is a monotonically decreasing function, i.e., as the received signal power increases there is a smaller chance of missing the signal.

**Theorem 1:** Consider a generic detection algorithm that computes a test-statistic  $T(\mathbf{Y})$  and compares it to a detector threshold  $\lambda$  to decide whether the band is free to use. Assume that the detection algorithm satisfies the following specifications:

- The mis-detection probability function (defined in (9)) satisfies,  $P_{MD}(-116) \leq 0.1$ .
- $P_{MD}(p)$  is a monotonically decreasing function of  $p$ .
- The probability of false-alarm (defined in (9)) satisfies  $P_{FA} \leq 0.1$ .

Assume that the nominal distribution (to compute WPAR) for the received signal power  $P$  is  $\mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(r)$  is a deterministic monotonically decreasing function of  $r$ . Furthermore, assume that the set of distributions  $\mathbb{F}_r$ , that the primary trusts (to compute  $F_{HI}$ ) for the received signal power  $P$  satisfies the single-quantile model in Definition 4. That is, any distribution  $F_r \in \mathbb{F}_r$  satisfies<sup>15</sup>

$$\mathcal{P}_{F_r}(P < -116) = \beta(r), \quad (10)$$

where  $\beta(r) = 1 - \mathcal{Q}\left(\frac{-116 - \mu(r)}{\sigma}\right)$ . Then, we have

$$\begin{aligned} F_{HI} &= 0.9\beta(r_n) + 0.1, \\ P_{FH}(r) &\leq \beta(r) + 0.1, \end{aligned} \quad (11)$$

*Proof:* The secondary user can use any detection algorithms as long as it meets the specifications given in the statement of

<sup>14</sup>The specified sensitivity of -116 dBm was based on the observation that it is easier (think shorter verification times) to verify a probability specification of 0.9 than it is to verify a probability specification of 0.999. Furthermore, there was an expectation that detector performance would monotonically improve with increased received power. Hence, a detector that demonstrated a probability of detection of 0.9 at -116 dBm would (hopefully) demonstrate a much higher detection probability at -110 dBm [58].

<sup>15</sup>Since only the -116 dBm level is specified, it is natural to assume that the primary only has confidence in a single-quantile that corresponds to that level.

the Theorem. To compute the fear of harmful interference to the primary user, one must consider the worst-possible detection algorithm satisfying the given specifications.

Let  $\mathcal{D}$  denote the set of all detection algorithms satisfying the specifications given in the statement of the theorem. Then, the fear of harmful interference is

$$\begin{aligned}
F_{HI} &= \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r} \sup_{D \in \mathcal{D}} \mathbb{E}_{F_r} [P_{MD}^D(P)] \\
&\stackrel{(a)}{=} \sup_{0 \leq r \leq r_n} \sup_{D \in \mathcal{D}} P_{MD}^D(-\infty) \mathcal{P}(P < -116) + P_{MD}^D(-116) \mathcal{P}(P \geq -116) \\
&\stackrel{(b)}{=} \sup_{0 \leq r \leq r_n} \sup_{D \in \mathcal{D}} [(1 - P_{FA}^D) \mathcal{P}(P < -116) + P_{MD}^D(-116) \mathcal{P}(P \geq -116)] \\
&\stackrel{(c)}{=} \sup_{0 \leq r \leq r_n} [\beta(r) + 0.1(1 - \beta(r))] \\
&= \sup_{0 \leq r \leq r_n} (0.9\beta(r) + 0.1) \\
&\stackrel{(d)}{=} 0.9\beta(r_n) + 0.1.
\end{aligned}$$

In the above chain of equalities the superscript  $D$  is used to denote a detection algorithm from the class of allowed detection algorithms  $\mathcal{D}$ . Equality (a) follows from the fact that the maximizing distribution  $F_r^* \in \mathbb{F}_r$  corresponds to placing a mass of  $\beta(r)$  at  $-\infty$  and  $(1 - \beta(r))$  at  $-116$  dBm. This is the maximizing distribution irrespective of the actual detection algorithm  $D \in \mathcal{D}$ . This is because  $P_{MD}^D(p)$  is a monotonically decreasing function of  $p$ , for all  $D \in \mathcal{D}$ . Equality (b) follows from the fact that  $P_{MD}^D(-\infty)$  is the mis-detection probability when the signal is absent ( $p = -\infty$ ). This corresponds to the event when noise-only received signal samples do not cause a false-alarm. Hence,  $P_{MD}^D(-\infty) = 1 - P_{FA}^D$ . Equality (c) follows from the fact that  $\sup_{D \in \mathcal{D}} (1 - P_{FA}^D) = 1$ , and  $\sup_{D \in \mathcal{D}} P_{MD}^D(-116) = 0.1$ . Finally, equality (d) follows from the fact that  $\beta(r)$  is a monotonically increasing function.

Now, for any  $D \in \mathcal{D}$ , the probability of finding a hole is given by

$$\begin{aligned}
P_{FH}(r) &= \mathbb{E}_P [\mathcal{P}(T^D(\mathbf{Y}) < \lambda | P)] \\
&= \mathbb{E}_P [P_{MD}^D(P)] \\
&\stackrel{(e)}{\leq} P_{MD}^D(-\infty) \mathcal{P}(P < -116) + P_{MD}^D(-116) \mathcal{P}(P \geq -116) \\
&\stackrel{(f)}{\leq} \beta(r) + 0.1, \quad \text{for } r > r_n.
\end{aligned} \tag{12}$$

The bound in (e) follows from the fact that the function  $P_{MD}^D(p) \leq P_{MD}^D(-\infty)$ , for  $-\infty < p < -116$ , and  $P_{MD}^D(p) \leq P_{MD}^D(-116)$ , for  $-116 \leq p < \infty$ . These inequalities follow from the fact that  $P_{MD}^D(p)$  is a monotonically decreasing function of  $p$ . The bound in (f) follows from observing that  $P_{MD}^D(-\infty) \leq 1$ ,  $\mathcal{P}(P < -116) := \beta(r)$ ,  $P_{MD}^D(-116) \leq 0.1 \quad \forall D \in \mathcal{D}$ , and  $\mathcal{P}(P \geq -116) \leq 1$ . ■

Shockingly, there is a benefit from missed detections above in step (f) of (12)! This suggests that a clever detector designer would do well to introduce intentional missed detections to improve performance while still meeting the official specification.

This calls into question the unspoken assumption that deployed detector implementations would have better probabilities of missed detection when the primary signal is stronger than  $-116$  dBm.

Using (12) in the definition of WPAR (See (5)) and applying our nominal model gives a  $WPAR \leq 0.16$ . This clearly shows that while the  $-116$  dBm requirement seems very conservative, the detector specification is actually not very safe and simultaneously has a poor area recovery irrespective of the actual detector used. In the worst-case, the signal can indeed fall as low as  $-116$  dBm at the no-talk radius. However in the average case the signal is a lot stronger and this leads to a lot of valuable area going unrecovered.

### B. The radiometer

The radiometer collects the samples of the received signal  $Y[n]$ , computes its empirical power and compares it to a detection threshold. The test-statistic for the radiometer can be written as

$$T(\mathbf{Y}) = \frac{1}{N} \sum_{n=1}^N |Y[n]|^2 \underset{D=0}{\overset{D=1}{\leq}} \lambda, \quad (13)$$

where  $\lambda$  is the design parameter and is called the detector threshold. Here,  $Y[n] = X[n] + W[n]$ , where  $X[n]$  is the faded primary signal at time  $n$ , and  $W[n]$  is the background noise at time  $n$ . For convenience assume that all  $W[n]$  are independent and identically distributed as  $\mathcal{N}(0, \sigma_w^2)$ . Also, let  $N$  be the total number of samples that are collected for sensing.

**Theorem 2:** Consider the radiometer whose test-statistic is defined in (13). Let  $P$  denote the average received primary signal power in the Decibel scale, i.e.,  $P = 10 \log_{10} \left( \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{n=1}^N |X[n]|^2 \right)$ . Let  $\mathbb{F}_r$  be the set of possible distributions for  $P$  at a distance of  $r$  from the primary transmitter.

Assume that the received power distribution is completely known and is given by  $P \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(\cdot)$  is a known monotonically decreasing function. This corresponds to the case of total consensus between primary and secondary and  $\mathbb{F}_r$  contains just the nominal model.

In this case, the safety/performance of the radiometer given in (13) is

$$\begin{aligned} F_{HI}^{ck} &= \int_{-\infty}^{\infty} \left[ 1 - \mathcal{Q} \left( \frac{\lambda - (10^{\frac{P}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}} (10^{\frac{P}{10}} + \sigma_w^2)} \right) \right] \cdot \frac{1}{\sqrt{2\pi\sigma^2}} \exp^{-\frac{(p - \mu(r_n))^2}{2\sigma^2}} dp + O\left(\frac{1}{\sqrt{N}}\right), \\ P_{FH}(r) &= \int_{-\infty}^{\infty} \left[ 1 - \mathcal{Q} \left( \frac{\lambda - (10^{\frac{P}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}} (10^{\frac{P}{10}} + \sigma_w^2)} \right) \right] \cdot \frac{1}{\sqrt{2\pi\sigma^2}} \exp^{-\frac{(p - \mu(r))^2}{2\sigma^2}} dp + O\left(\frac{1}{\sqrt{N}}\right), \end{aligned} \quad (14)$$

and the WPAR is given by

$$WPAR^{ck} = \int_{r_n}^{\infty} w(r) P_{FH}(r) r dr$$

*Proof:* As the received power distribution is completely known, the fear of harmful interference is given by

$$F_{HI}^{ck} = \mathbb{E}_P [\mathcal{P}(T(\mathbf{Y}) < \lambda | P)], \quad (15)$$

where  $P \sim \mathcal{N}(\mu(r_n), \sigma^2)$ . Let  $P = p$  be a given received power realization, then using the Central Limit Theorem (CLT) we can approximate  $T(\mathbf{Y}) \sim \mathcal{N}(10^{\frac{p}{10}} + \sigma_w^2, \frac{2}{N}[10^{\frac{p}{10}} + \sigma_w^2]^2)$  [16]. Furthermore, if  $F_T^N(x)$  is the CDF of  $\frac{T(\mathbf{Y}) - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}[10^{\frac{p}{10}} + \sigma_w^2]}}$ , then the Berry-Esseen Theorem (see Theorem 2.4.9 in [59]) about the convergence of the CLT gives us

$$|F_T^N(x) - G(x)| \leq \frac{c}{\sqrt{N}}, \quad \forall x \in (-\infty, \infty)$$

where  $G(x)$  is the CDF of a  $\mathcal{N}(0, 1)$  distribution, and  $c > 0$  is a known constant.

Therefore,

$$\mathcal{P}(T(\mathbf{Y}) < \lambda | P = p) = 1 - \mathcal{Q}\left(\frac{\lambda - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}(10^{\frac{p}{10}} + \sigma_w^2)}}\right) + O\left(\frac{1}{\sqrt{N}}\right). \quad (16)$$

Using (16) in (15) we get

$$\begin{aligned} F_{HI}^{ck} &= \int_{-\infty}^{\infty} \left[ 1 - \mathcal{Q}\left(\frac{\lambda - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}(10^{\frac{p}{10}} + \sigma_w^2)}}\right) + O\left(\frac{1}{\sqrt{N}}\right) \right] \cdot \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{(p - \mu(r_n))^2}{2\sigma^2}\right) dp \\ &= \int_{-\infty}^{\infty} \left[ 1 - \mathcal{Q}\left(\frac{\lambda - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}(10^{\frac{p}{10}} + \sigma_w^2)}}\right) \right] \cdot \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{(p - \mu(r_n))^2}{2\sigma^2}\right) dp + O\left(\frac{1}{\sqrt{N}}\right). \end{aligned} \quad (17)$$

The probability of finding a hole at a distance  $r$  from the transmitter is given by

$$P_{FH}(r) = \mathbb{E}_P[\mathcal{P}(T(\mathbf{Y}) < \lambda | P)], \quad (18)$$

where  $P \sim \mathcal{N}(\mu(r), \sigma^2)$ . Therefore,

$$P_{FH}(r) = \int_{-\infty}^{\infty} \left[ 1 - \mathcal{Q}\left(\frac{\lambda - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}(10^{\frac{p}{10}} + \sigma_w^2)}}\right) \right] \cdot \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{(p - \mu(r))^2}{2\sigma^2}\right) dp + O\left(\frac{1}{\sqrt{N}}\right). \quad (19)$$

Substituting (19) in (5) gives us the expression for WPAR

$$WPAR^{ck} = \int_{r_n}^{\infty} w(r) \left( \int_{-\infty}^{\infty} \left[ 1 - \mathcal{Q}\left(\frac{\lambda - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}(10^{\frac{p}{10}} + \sigma_w^2)}}\right) \right] \cdot \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{(p - \mu(r))^2}{2\sigma^2}\right) dp \right) r dr + O\left(\frac{1}{\sqrt{N}}\right). \quad (20)$$

■

Note that the expressions for the performance/safety of the radiometer in Theorem 2 contain error terms from the CLT approximation. If one wishes to compute exact expressions then they must use the Chi-squared distribution for the test-statistic  $T(\mathbf{Y})$ . In the rest of the paper, we omit the error terms arising due to the CLT approximation. This is done to keep the mathematical equations simple.

Theorem 2 gives us the safety/performance of a radiometer with complete distributional knowledge. We now give the safety/performance under the single-quantile model of Section III-D for the received signal distribution.

**Theorem 3:** Consider the radiometer whose test-statistic is defined in (13). Let  $P$  denote the average received primary

signal power in the Decibel scale, i.e.,  $P = 10 \log_{10} \left( \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{n=1}^N |X[n]|^2 \right)$ . Let  $\mathbb{F}_r$  be the set of possible distributions for  $P$  at a distance of  $r$  from the primary transmitter. Assume that the uncertain set  $\mathbb{F}_r$  satisfies the single-quantile model of Section III-D. That is, given a  $0 \leq \beta \leq 1$ , the primary agrees on a threshold  $\gamma(r, \beta)$  such that for every distribution  $F_r \in \mathbb{F}_r$ ,  $\mathcal{P}_{F_r}(P < \gamma(r, \beta)) = \beta$ , where  $\gamma(r, \beta) = \sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r)$ .

In this case, the fear of harmful interference is given by

$$F_{HI}^{sq} = \beta \left[ 1 - \mathcal{Q} \left( \frac{\lambda - \sigma_w^2}{\sqrt{\frac{2}{N} \sigma_w^2}} \right) \right] + (1 - \beta) \left[ 1 - \mathcal{Q} \left( \frac{\lambda - (10^{\frac{\gamma(r_n, \beta)}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N} (10^{\frac{\gamma(r_n, \beta)}{10}} + \sigma_w^2)}} \right) \right], \quad (21)$$

where  $\gamma(r_n, \beta) = \sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r_n)$ . The WPAR performance is same as Eqn. (20) in Theorem 2.

*Proof:* In the single-quantile model, the fear of harmful interference ( $F_{HI}$ ) is then given by

$$F_{HI}^{sq} = \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r} \mathbb{E}_{F_r} [\mathcal{P}(T(\mathbf{Y}) < \lambda | P = p)]. \quad (22)$$

For a given received power realization  $P = p$ , the CLT gives us  $T(\mathbf{Y}) \sim \mathcal{N} \left( 10^{\frac{p}{10}} + \sigma_w^2, \frac{2}{N} [10^{\frac{p}{10}} + \sigma_w^2]^2 \right)$  [16]. Therefore,

$$\mathcal{P}(T(\mathbf{Y}) < \lambda | P = p) = 1 - \mathcal{Q} \left( \frac{\lambda - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N} (10^{\frac{p}{10}} + \sigma_w^2)}} \right). \quad (23)$$

So,

$$\begin{aligned} F_{HI}^{sq} &= \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r} \mathbb{E}_{F_r} [\mathcal{P}(T(\mathbf{Y}) < \lambda | P = p)] \\ &\stackrel{(a)}{=} \sup_{0 \leq r \leq r_n} [\beta \mathcal{P}(T(\mathbf{Y}) < \lambda | P = -\infty) + (1 - \beta) \mathcal{P}(T(\mathbf{Y}) < \lambda | P = \gamma(r, \beta))] \\ &\stackrel{(b)}{=} [\beta \mathcal{P}(T(\mathbf{Y}) < \lambda | P = -\infty) + (1 - \beta) \mathcal{P}(T(\mathbf{Y}) < \lambda | P = \gamma(r_n, \beta))]. \end{aligned} \quad (24)$$

The equality in (a) follows from the fact that the optimizing distribution  $F_r^* \in \mathbb{F}_r$  has a mass of  $\beta$  at  $-\infty$  and has a mass of  $(1 - \beta)$  at  $\gamma(r, \beta)$ . This is because, from (23) we can see that  $\mathcal{P}(T(\mathbf{Y}) < \lambda | P = p)$  is a monotonically decreasing function of  $p$ . The equality in (b) reveals that the worst-case location corresponds to  $r = r_n$ . This follows from these observations. Firstly,  $\mathcal{P}(T(\mathbf{Y}) < \lambda | P = -\infty)$  is independent of  $r$  (use  $p = -\infty$  in (23)). Secondly,  $\mathcal{P}(T(\mathbf{Y}) < \lambda | P = \gamma(r, \beta))$  monotonically increases with decreasing  $\gamma(r, \beta)$ , whereas  $\gamma(r, \beta)$  monotonically decreases with increasing  $r$  (recall,  $\gamma(r, \beta) = \sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r)$ , and  $\mu(r)$  decreases with increasing  $r$ ). So,

$$F_{HI}^{sq} = \beta \left[ 1 - \mathcal{Q} \left( \frac{\lambda - \sigma_w^2}{\sqrt{\frac{2}{N} \sigma_w^2}} \right) \right] + (1 - \beta) \left[ 1 - \mathcal{Q} \left( \frac{\lambda - (10^{\frac{\gamma(r_n, \beta)}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N} (10^{\frac{\gamma(r_n, \beta)}{10}} + \sigma_w^2)}} \right) \right], \quad (25)$$

where  $\gamma(r_n, \beta) = \sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r_n)$ . ■

Note that the secondary user has two parameters to adjust. It can adjust the threshold  $\lambda$  on its own and it can negotiate with the regulator/primary regarding the appropriate value for  $\beta$ . We assume that it does both and satisfies (25). The optimal

$\beta$  and  $\lambda$  are chosen to maximize  $WPAR^{ck}$  (See Eqn. (20)). This can be done numerically. Figure 7 shows the resulting safety/performance tradeoff for a single radio with both a finite and infinite number of samples. From Figure 7 we can see that the impact of the uncertainty is substantial when the sensing time is finite.

A special limiting case of interest is when the number of samples available for detection is infinite. This allows us to isolate the effect of fading/shadowing from the effect of finite samples. We call this a ‘perfect’ radiometer (in general a single-user perfect detector). The test-statistic for a perfect radiometer is  $T^{per}(\mathbf{Y}) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{n=1}^N |Y[n]|^2$ . As  $Y[n]$  are independent and identically (*iid*) distributed random variables, the strong law of large numbers implies  $\frac{1}{N} \sum_{n=1}^N |Y[n]|^2 \xrightarrow{a.s.} 10^{\frac{p}{10}} + \sigma_w^2$ , where  $p$  (in dBm) is the average received signal power. Therefore, the perfect radiometer decides whether the band is used/unused according to the following rule

$$\begin{aligned} T^{per}(\mathbf{Y}) &= 10^{\frac{P}{10}} + \sigma_w^2 \underset{D=0}{\overset{D=1}{\gtrless}} \lambda \\ &\Leftrightarrow P \underset{D=0}{\overset{D=1}{\gtrless}} 10 \log_{10}(\lambda - \sigma_w^2), \end{aligned} \quad (26)$$

We now derive the safety/performance of the perfect radiometer.

**Theorem 4:** Consider a perfect radiometer, whose test-statistic is defined in (26), where  $P$  is the received signal power,  $\tilde{\lambda} := 10 \log_{10}(\lambda - \sigma_w^2)$  is the detection threshold and  $\mathbb{F}_r$  is the set of possible distributions for  $P$  at a distance of  $r$  from the primary transmitter.

- **A:** Assume that the received power distribution is completely known ( $\mathbb{F}_r$  is a singleton) and is given by  $P \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(\cdot)$  is a known monotonically decreasing function. Then, the safety/performance is given by

$$\begin{aligned} F_{HI}^{per,ck} &= 1 - \mathcal{Q}\left(\frac{\tilde{\lambda} - \mu(r_n)}{\sigma}\right), \\ WPAR^{per,ck} &= \int_{r_n}^{\infty} w(r) \left[1 - \mathcal{Q}\left(\frac{\tilde{\lambda} - \mu(r)}{\sigma}\right)\right] r \, dr. \end{aligned} \quad (27)$$

- **B:** Assume that the uncertain set  $\mathbb{F}_r$  satisfies the single-quantile model of Section III-D. That is, given a  $0 \leq \beta \leq 1$ , the primary agrees on a threshold  $\gamma(r, \beta)$  such that for every distribution  $F_r \in \mathbb{F}_r$ ,  $\mathcal{P}_{F_r}(P < \gamma(r, \beta)) = \beta$ , where  $\gamma(r, \beta) = \sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r)$ . Then, the fear of harmful interference is given by

$$F_{HI}^{per,sq} = \begin{cases} \beta & \text{if } \tilde{\lambda} \leq \gamma(r_n, \beta) \\ 1 & \text{otherwise.} \end{cases} \quad (28)$$

The WPAR in this case is same as in the complete knowledge case (See Eqn. (27)).



*Proof:* **Proof of (A):** The fear of harmful interference is given by

$$\begin{aligned}
F_{HI}^{per,ck} &:= \sup_{0 \leq r \leq r_n} \mathcal{P}(P < \tilde{\lambda}) \\
&\stackrel{(a)}{=} \sup_{0 \leq r \leq r_n} \left[ 1 - \mathcal{Q}\left(\frac{\tilde{\lambda} - \mu(r)}{\sigma}\right) \right] \\
&\stackrel{(b)}{=} 1 - \mathcal{Q}\left(\frac{\tilde{\lambda} - \mu(r_n)}{\sigma}\right),
\end{aligned} \tag{29}$$

where (a) follows from the fact that  $P \sim \mathcal{N}(\mu(r), \sigma^2)$  and (b) follows from the monotonicity of the  $\mathcal{Q}(\cdot)$  function. Similarly, the probability of finding a hole is given by

$$\begin{aligned}
P_{FH}(r) &= \mathcal{P}(P < \tilde{\lambda}) \\
&= 1 - \mathcal{Q}\left(\frac{\tilde{\lambda} - \mu(r)}{\sigma}\right),
\end{aligned}$$

Substituting the above expression for  $P_{FH}(r)$  in (5) gives us the desired result.

**Proof of (B):** Under the single-quantile model for  $\mathbb{F}_r$ , the fear of harmful interference is given by

$$F_{HI}^{per,sq} := \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r} \mathcal{P}(P < \tilde{\lambda}). \tag{30}$$

We know that  $\mathcal{P}(P < \gamma(r, \beta)) = \beta$ . If  $\gamma(r, \beta) \geq \tilde{\lambda}$  then clearly the distribution  $F_r^* \in \mathbb{F}_r$ , maximizing  $\sup_{F_r \in \mathbb{F}_r} \mathcal{P}(P < \tilde{\lambda})$  has mass  $\beta$  at  $-\infty$  and hence  $\sup_{F_r \in \mathbb{F}_r} \mathcal{P}(P < \tilde{\lambda}) = \beta$ . On the other hand if  $\gamma(r, \beta) < \tilde{\lambda}$  then the distribution having mass of  $\beta$  at  $-\infty$  and mass of  $(1 - \beta)$  at  $\gamma(r, \beta)$  belongs to the set  $\mathbb{F}_r$  and for this distribution  $\mathcal{P}(P < \tilde{\lambda}) = 1$ . Therefore,

$$\sup_{F_r \in \mathbb{F}_r} \mathcal{P}(P < \tilde{\lambda}) = \begin{cases} \beta & \text{if } \tilde{\lambda} \leq \gamma(r, \beta) \\ 1 & \text{otherwise.} \end{cases} \tag{31}$$

Note that  $\gamma(r, \beta) := \sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r)$  is monotonically decreasing in  $r$ . Using this fact in (31), we get

$$F_{HI}^{per,sq} := \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r} \mathcal{P}(P < \tilde{\lambda}) = \begin{cases} \beta & \text{if } \tilde{\lambda} \leq \gamma(r_n, \beta) \\ 1 & \text{otherwise.} \end{cases}$$

■

**Corollary 1:** Consider the perfect radiometer under the single-quantile uncertainty model for  $\mathbb{F}_r$ . For a given choice of target fear of harmful interference  $F_{HI}^t$ , the optimal  $\beta^*$  and  $\tilde{\lambda}^*$  that maximizes  $WPAR^{per,sq}$  subject to  $F_{HI}^{per,sq} \leq F_{HI}^t$  is given by

$$\beta^* = F_{HI}^t, \quad \tilde{\lambda}^* = \sigma \mathcal{Q}^{-1}(1 - F_{HI}^t) + \mu(r_n). \tag{32}$$

Hence,  $F_{HI}^t = \mathcal{Q}\left(\frac{\lambda^* - \mu(r_n)}{\sigma}\right)$ , which is the same as the safety performance given in (27) for the perfect radiometer under complete distributional knowledge.

*Proof:* From (28) it is clear that, to meet the constraint  $F_{HI}^{per,sq} \leq F_{HI}^t$  we must have  $\beta \leq F_{HI}^t$  and  $\gamma(r_n, \beta) \geq \tilde{\lambda}$ .

Therefore, the optimization problem is reduced to

$$\sup_{\beta, \tilde{\lambda}} \left[ \int_{r_n}^{\infty} w(r) \left[ 1 - \mathcal{Q} \left( \frac{\tilde{\lambda} - \mu(r)}{\sigma} \right) \right] r dr \right] : \quad \text{s.t. } \beta \leq F_{HI}^t, \quad \tilde{\lambda} \leq \sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r_n). \quad (33)$$

Note that the objective function is monotonically increasing function of  $\tilde{\lambda}$ . This is because  $\left[ 1 - \mathcal{Q} \left( \frac{\tilde{\lambda} - \mu(r)}{\sigma} \right) \right]$  is monotonically increasing with  $\tilde{\lambda}$  and  $w(r) \geq 0$ . Also, note that the constraint on  $\tilde{\lambda}$ ,  $\sigma \mathcal{Q}^{-1}(1 - \beta) + \mu(r_n)$  is monotonically increasing with  $\beta$ . These two observations imply that the optimizing  $\beta^*$  and  $\tilde{\lambda}^*$  are the extreme values of the constraint functions, i.e.,  $\beta^* = F_{HI}^t$  and  $\tilde{\lambda}^* = \sigma \mathcal{Q}^{-1}(1 - F_{HI}^t) + \mu(r_n)$ . ■

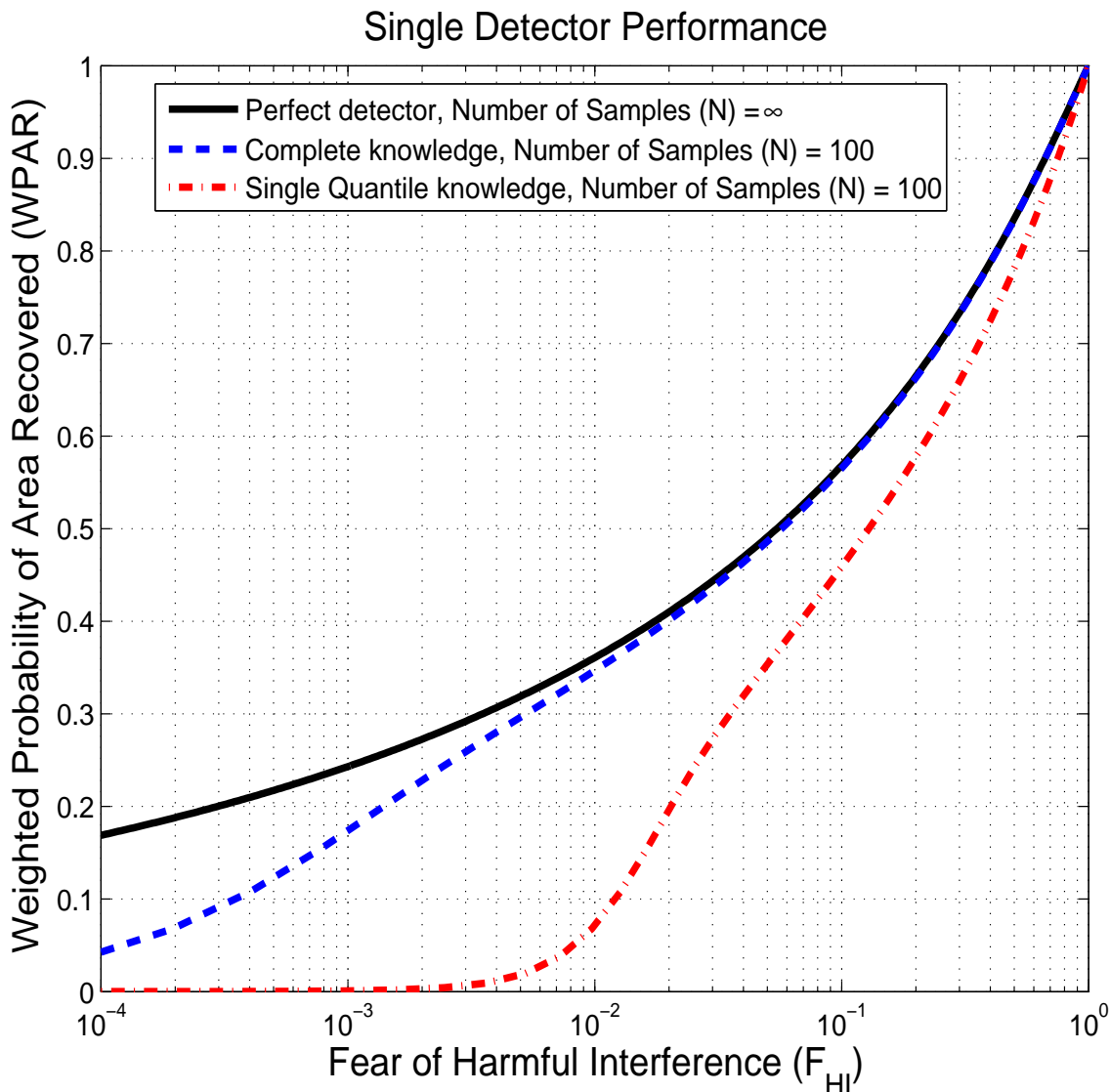


Fig. 7. Performance of a perfect detector (infinite samples) as compared with a radiometer using a finite number of samples.

### C. The value of additional samples

Next we look the gap between the safety-constrained performance with only a single (but optimized) trusted quantile and what can be achieved with the entire fading distribution being trusted. The first step is to increase the sensing duration. Figure 8 shows the gap in performance as the number of samples  $N$  is scaled but the  $F_{HI}$  of the system is constrained to be  $10^{-3}$ . An infinite number of samples leads to a perfect detector, and it turns out that having a single trusted quantile leads to the same performance as having complete distributional knowledge. This is because that single-quantile can be chosen in an optimal fashion based on the target  $F_{HI}$  itself. Hence the two curves achieve the same WPAR value as the number of samples are scaled up. However, they need different numbers of samples. If the entire distribution were trusted, a single radio only needs  $\sim 10^3$  samples whereas  $> 10^6$  samples are needed if only a single-quantile can be trusted. We now give a mathematical proof for the convergence result observed in Figure 8.

**Theorem 5:** Consider a perfect radiometer with test-statistic  $T^{per}(\mathbf{Y}) := \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{n=1}^N |Y[n]|^2 = 10^{\frac{P}{10}} + \sigma_w^2$ , where  $P$  (in dBm) is the received signal power and  $\sigma_w^2$  is the variance of the noise samples. Assume that the received signal power distribution is completely known and  $P \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(\cdot)$  is a monotonically decreasing deterministic function of the distance  $r$ . Set the detector threshold  $\lambda_0$  (in linear scale) (See Eqn. (26)) so as to meet a given target fear of harmful interference,  $F_{HI}^t$ , i.e.,

$$\mathbb{E}_{F_{r_n}} [\mathcal{P}(T^{per}(\mathbf{Y}) < \lambda_0 | P)] = F_{HI}^t, \quad (34)$$

where  $F_{r_n}(\cdot)$  is a Gaussian CDF function with mean  $\mu(r_n)$  and variance  $\sigma^2$ , i.e., the cumulative distribution function for the received power  $P$  at  $r_n$ .

The corresponding WPAR can be written as:

$$\begin{aligned} P_{FH}^{per,ck}(r) &= \mathbb{E}_{F_r} [\mathcal{P}(T^{per}(\mathbf{Y}) < \lambda_0 | P)], \\ WPAR^{per,ck} &= \int_{r_n}^{\infty} w(r) P_{FH}^{per,ck}(r) r dr, \end{aligned} \quad (35)$$

where  $F_r$  is a Gaussian CDF function with mean  $\mu(r)$  and variance  $\sigma^2$ .

Next, consider a radiometer with complete knowledge of the signal distribution but restricted to using  $N$  samples, i.e., its test-statistic is given by  $T_N(\mathbf{Y}) := \frac{1}{N} \sum_{n=1}^N |Y[n]|^2$ . To meet  $F_{HI}^t$ , such a detector must set its detector threshold  $\lambda_N$  such that,

$$\mathbb{E}_{F_{r_n}} [\mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P)] = F_{HI}^t. \quad (36)$$

As in the perfect detector case,  $F_{r_n}(\cdot)$  is a Gaussian CDF function with mean  $\mu(r_n)$  and variance  $\sigma^2$ . The corresponding WPAR can be written as:

$$\begin{aligned} P_{FH}^{ck}(r, N) &= \mathbb{E}_{F_r} [\mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P)], \\ WPAR^{ck}(N) &= \int_{r_n}^{\infty} w(r) P_{FH}^{ck}(r, N) r dr, \end{aligned} \quad (37)$$

where  $F_r$  is a Gaussian CDF function with mean  $\mu(r)$  and variance  $\sigma^2$ .

Then,

$$\lim_{N \rightarrow \infty} WPAR^{ck}(N) = WPAR^{per,ck}. \quad (38)$$

*Proof:* From (35) and (37),

$$\begin{aligned} WPAR^{ck}(N) &\xrightarrow{N \rightarrow \infty} WPAR^{per,ck} \\ \text{if } P_{FH}^{ck}(r, N) &\xrightarrow{N \rightarrow \infty} P_{FH}^{per,ck}(r) \quad \forall r \geq r_n \\ \text{if } \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) &\xrightarrow{N \rightarrow \infty} \mathcal{P}(T^{per}(\mathbf{Y}) < \lambda_0 | P = p) \quad \forall p. \end{aligned} \quad (39)$$

By definition,  $T^{per}(\mathbf{Y}) = 10^{\frac{p}{10}} + \sigma_w^2$ . Therefore,

$$\begin{aligned} \mathcal{P}(T^{per}(\mathbf{Y}) < \lambda_0 | P = p) &= \mathcal{P}\left(10^{\frac{p}{10}} + \sigma_w^2 < \lambda_0 | P = p\right) \\ &= \mathcal{P}\left(10^{\frac{p}{10}} + \sigma_w^2 < \lambda_0\right) \\ &= J(p, \lambda_0), \end{aligned} \quad (40)$$

where

$$J(p, \lambda_0) := \begin{cases} 1 & \text{if } 10^{\frac{p}{10}} < \lambda_0 - \sigma_w^2 \\ 0 & \text{if } 10^{\frac{p}{10}} \geq \lambda_0 - \sigma_w^2. \end{cases} \quad (41)$$

From (39) with (41), it is sufficient to show that

$$\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) = J(p, \lambda_0). \quad (42)$$

**Lemma 1:** Assume  $\lim_{N \rightarrow \infty} \lambda_N = \lambda_\infty$ . Then,

$$\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) = J(p, \lambda_\infty). \quad (43)$$

*Proof:* Let  $(10^{\frac{p}{10}} + \sigma_w^2) < \lambda_\infty$ . Fix  $\epsilon_1 = \frac{\lambda_\infty - (10^{\frac{p}{10}} + \sigma_w^2)}{2} > 0$ . Since  $\lambda_N \xrightarrow{N \rightarrow \infty} \lambda_\infty$ ,  $\exists N_1 > 0$  such that  $|\lambda_\infty - \lambda_N| \leq \epsilon_1$  for all  $N > N_1$ .

Let  $N > N_1$ . Then, from (23) we have

$$\begin{aligned} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) &= 1 - \mathcal{Q}\left(\frac{\lambda_N - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}(10^{\frac{p}{10}} + \sigma_w^2)}}\right) \\ &\stackrel{(a)}{\geq} 1 - \mathcal{Q}\left(\frac{\epsilon_1}{\sqrt{\frac{2}{N}(10^{\frac{p}{10}} + \sigma_w^2)}}\right). \end{aligned} \quad (44)$$

(a) follows from the fact that  $\mathcal{Q}(\cdot)$  is a monotonically decreasing function and that for  $N > N_1$ ,  $\lambda_N \geq \lambda_\infty - \epsilon_1$ , which

implies  $\lambda_N - (10^{\frac{p}{10}} + \sigma_w^2) \geq \lambda_\infty - (10^{\frac{p}{10}} + \sigma_w^2) - \epsilon_1 = 2\epsilon_1 - \epsilon_1 = \epsilon_1$ . Now, taking limits as  $N \rightarrow \infty$  in (44) we get

$$\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) \geq 1 - \mathcal{Q}(\infty) = 1, \quad (45)$$

which implies  $\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) = 1$  for  $(10^{\frac{p}{10}} + \sigma_w^2) < \lambda_\infty$ .

Now, let  $(10^{\frac{p}{10}} + \sigma_w^2) \geq \lambda_\infty$ . Fix  $\epsilon_2 = \frac{(10^{\frac{p}{10}} + \sigma_w^2) - \lambda_\infty}{2} > 0$ . Since  $\lambda_N \xrightarrow{N \rightarrow \infty} \lambda_\infty$ ,  $\exists N_2 > 0$  such that  $|\lambda_\infty - \lambda_N| \leq \epsilon_2$  for all  $N > N_2$ .

Let  $N > N_2$ . Then, from (23) we have

$$\begin{aligned} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) &= 1 - \mathcal{Q}\left(\frac{\lambda_N - (10^{\frac{p}{10}} + \sigma_w^2)}{\sqrt{\frac{2}{N}}(10^{\frac{p}{10}} + \sigma_w^2)}\right) \\ &\stackrel{(b)}{\leq} 1 - \mathcal{Q}\left(\frac{-\epsilon_2}{\sqrt{\frac{2}{N}}(10^{\frac{p}{10}} + \sigma_w^2)}\right). \end{aligned} \quad (46)$$

(b) follows from the fact that  $\mathcal{Q}(\cdot)$  is a monotonically decreasing function and that for  $N > N_2$ ,  $\lambda_N \leq \lambda_\infty + \epsilon_2$ , which implies  $\lambda_N - (10^{\frac{p}{10}} + \sigma_w^2) \leq \lambda_\infty - (10^{\frac{p}{10}} + \sigma_w^2) + \epsilon_2 = -2\epsilon_2 + \epsilon_2 = -\epsilon_2$ . Now, taking limits as  $N \rightarrow \infty$  in (46) we get

$$\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) \leq 1 - \mathcal{Q}(-\infty) = 0, \quad (47)$$

which implies  $\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) = 0$  for  $(10^{\frac{p}{10}} + \sigma_w^2) \geq \lambda_\infty$ .

Therefore, we have shown that  $\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) = J(p, \lambda_\infty)$ , which proves the lemma.  $\blacksquare$

From (36) we have

$$\int_{-\infty}^{\infty} [\mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p)] f(p) dp = F_{HI}^t, \quad (48)$$

where  $f(p) = \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{(p - \mu(r_n))^2}{2\sigma^2}\right)$  is the Gaussian probability density function. Taking limits as  $N \rightarrow \infty$  in (48), we get

$$\begin{aligned} \lim_{N \rightarrow \infty} \int_{-\infty}^{\infty} [\mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P)] f(p) dp &= F_{HI}^t \\ \stackrel{(a)}{\Rightarrow} \int_{-\infty}^{\infty} \left[ \lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P) \right] f(p) dp &= F_{HI}^t \\ &\stackrel{(b)}{\Rightarrow} \int_{-\infty}^{\infty} J(p, \lambda_\infty) f(p) dp = F_{HI}^t \\ &\Rightarrow 1 - \mathcal{Q}\left(\frac{\widetilde{\lambda}_\infty - \mu(r_n)}{\sigma}\right) = F_{HI}^t, \end{aligned} \quad (49)$$

where  $\widetilde{\lambda}_\infty = 10 \log_{10}(\lambda_\infty - \sigma_w^2)$ . In the above chain of implications, (a) follows by interchanging the order of integration and taking limits. This is justified by appealing to the Dominated Convergence Theorem [59]. In our case the sequence of functions  $\mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P)$  are dominated by the constant function 1. (b) follows from Lemma 1.

From (34) we have

$$F_{HI}^t = \mathbb{E}_{F_{r_n}} [\mathcal{P}(T^{per}(\mathbf{Y}) < \lambda_0 | P)]$$

$$\stackrel{(c)}{=} 1 - \mathcal{Q}\left(\frac{\tilde{\lambda}_0 - \mu(r_n)}{\sigma}\right), \quad (50)$$

where  $\tilde{\lambda}_0 = 10 \log_{10}(\lambda_0 - \sigma_w^2)$  and (c) follows from (29) in Theorem 4.

Now, comparing (49) and (50) we have  $\tilde{\lambda}_\infty = \tilde{\lambda}_0$ , which implies  $\lambda_\infty = \lambda_0$ . Using this fact in (43) gives us

$$\lim_{N \rightarrow \infty} \mathcal{P}(T_N(\mathbf{Y}) < \lambda_N | P = p) = J(p, \lambda_0), \quad (51)$$

which proves the theorem. ■

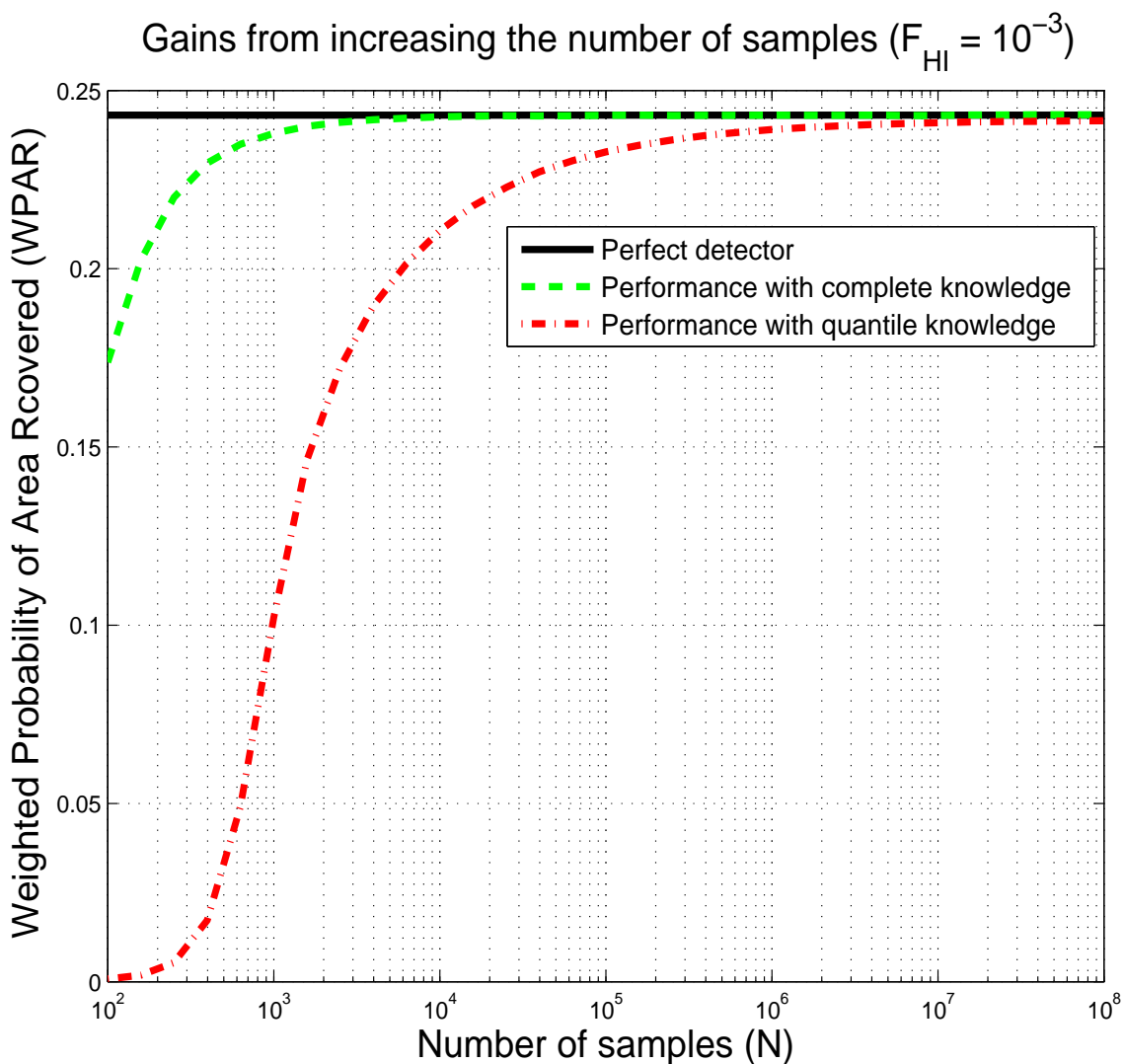


Fig. 8. Performance of a radiometer with finite samples approaches the performance of the perfect detector as samples are increased.

#### D. The value of additional consensus

The previous section shows that there is a clear value to agreeing on a single model for the entire distribution. However, this is likely to be impossible in practice. Instead, suppose that the primary user, secondary user, and regulators agreed on a few quantiles of the fading distribution instead of a single one.

Figure 9 shows the fear of harmful interference ( $F_{HI}$ ) for a fixed WPAR as the number of quantiles is increased while the sensing time is kept constant. Two methods for quantile selection are compared. In the first method the quantiles are chosen uniformly (e.g. if three quantiles were needed, select the 1/4th, 1/2 and 3/4th quantile). In the second method, the best additional quantile is chosen greedily given the choice of the previous quantiles. Both methods approach the same limit, but the greedy choice clearly performs better. The threshold used in this plot corresponds to a  $F_{HI}$  of 0.1 if the entire distribution is trusted. A moderate number of quantiles ( $\sim 10$ ) are needed for the safety to be reasonably close to the safety with complete distributional knowledge, for the same detection threshold.

If the  $F_{HI}$  were to be held constant, the WPAR performance would improve instead. By gaining additional consensus regarding the fading distribution, the sensing threshold can be set more aggressively without the fear of harmful interference. This aggressive threshold in turn increases the WPAR. We now give a mathematical proof of the convergence result observed in Figure 9.

**Theorem 6:** Consider a radiometer using  $N$  samples for detection. The test-statistic is given by  $T(\mathbf{Y}) = \frac{1}{N} \sum_{n=1}^N |Y[n]|^2$ . Set the detector threshold  $\lambda_0$  such that under complete distributional knowledge, a given target fear of harmful interference  $F_{HI}^t$  is met. That is,

$$\mathbb{E}_{F_{r_n}}[\mathcal{P}(T(\mathbf{Y}) < \lambda_0 | P)] = F_{HI}^t, \quad (52)$$

where  $F_{r_n}$  is a Gaussian CDF with mean  $\mu(r_n)$  and variance  $\sigma^2$ .

Now, we evaluate the safety performance of this detector (with detection threshold set at  $\lambda_0$ ) under limited distributional knowledge. Fix  $M > 0$ . Define  $\mathbb{F}_r^M$  to be the set of distributions satisfying the following properties

- Choose  $M$  quantization points  $(q_1, q_2, \dots, q_M) \in \mathbb{R}^M$  such that  $q_i = \sigma \mathcal{Q}^{-1} \left( 1 - \frac{i}{M+1} \right) + \mu(r)$ , for all  $i = 1, 2, \dots, M$ .
- Any cumulative distribution function  $F_r \in \mathbb{F}_r^M \Leftrightarrow \mathcal{P}_{F_r}(P < q_i) = \frac{i}{M+1}$ , for all  $i = 1, 2, \dots, M$ .

Let  $F_{HI}^M$  be the fear of harmful interference for the radiometer under the  $M$  uniform-quantile uncertainty model defined above. That is,

$$F_{HI}^M := \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r^M} \mathbb{E}_{F_r}[\mathcal{P}(T(\mathbf{Y}) < \lambda_0 | P)]. \quad (53)$$

Then,  $F_{HI}^M \xrightarrow{M \rightarrow \infty} F_{HI}^t$ .

*Proof:* Define,  $g(p) := \mathcal{P}(T(\mathbf{Y}) < \lambda_0 | P = p)$ . The exact expression for  $g(p)$  is derived in (16). Note that  $g(p)$  is a monotonically decreasing function of  $p$ . Now,

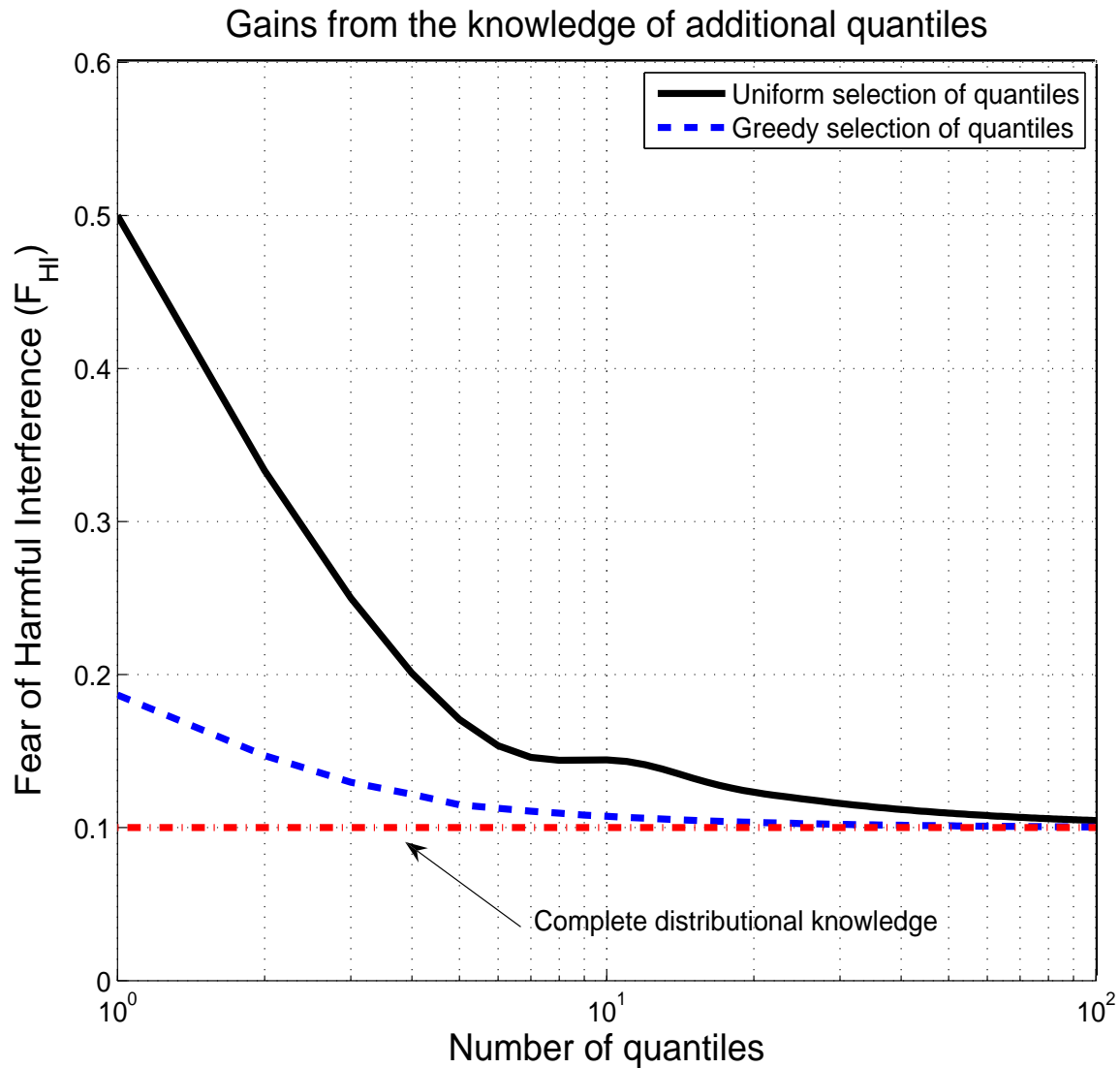


Fig. 9. The  $F_{HI}$  of an energy detector with 100 samples but distributional uncertainty approaches the  $F_{HI}$  with no uncertainty as the number of known quantiles is increased. Various ways of choosing quantiles show slightly different performance. The threshold used in this plot corresponds to a  $F_{HI}$  of .1 without distributional uncertainty.

$$\begin{aligned}
 F_{HI}^M &:= \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r^M} \mathbb{E}_{F_r} [\mathcal{P}(T(\mathbf{Y}) < \lambda_0 | P)] \\
 &= \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r^M} \mathbb{E}_{F_r} [g(P)] \\
 &\stackrel{(a)}{=} \sup_{0 \leq r \leq r_n} \mathbb{E}_{F_r^M} [g(P)] \\
 &\stackrel{(b)}{=} \mathbb{E}_{F_{r_n}^M} [g(P)],
 \end{aligned} \tag{54}$$



where the CDF  $F_r^M$  is defined as

$$F_r^M(p) := \begin{cases} \frac{1}{M+1} & \text{if } -\infty \leq p < q_1 \\ \frac{2}{M+1} & \text{if } q_1 \leq p < q_2 \\ \frac{3}{M+1} & \text{if } q_2 \leq p < q_3 \\ \dots & \\ 1 & \text{if } q_M \leq p < \infty. \end{cases} \quad (55)$$

That is, the CDF  $F_r^M(p)$  places uniform mass ( $\frac{1}{M+1}$ ) over each of the quantization points  $(-\infty, q_1, \dots, q_M)$ . In (54), (a) follows because  $F_r^M \in \mathbb{F}_r^M$  is the worst-case CDF. This is true because  $g(p)$  is a monotonically decreasing function and hence the CDF that maximizes  $E[g(P)]$  places all the mass within each quantization bin at the left most point in the bin. (b) follows from the observation that the fear of harmful interference is worst at the edge of the no-talk radius. This can be seen from the following argument. Evaluating  $\mathbb{E}_{F_r^M}[g(P)]$  in (54) using the CDF in (55), we get  $\mathbb{E}_{F_r^M}[g(P)] = \frac{1}{M+1} \sum_{i=0}^M g(q_i)$ , where  $q_0 = -\infty$ , and  $q_i := \sigma \mathcal{Q}^{-1}\left(1 - \frac{i}{M+1}\right) + \mu(r)$ , for  $1 \leq i \leq M$ . It is clear that  $q_0 \leq q_1 \leq \dots \leq q_M$  (because  $\mathcal{Q}(\cdot)$  is a monotonically decreasing function). Furthermore, both  $\mu(r)$  and  $g(p)$  are monotonically decreasing functions, so

$$\begin{aligned} \sup_{0 \leq r \leq r_n} \mathbb{E}_{F_{r_n}^M}[g(P)] &:= \sup_{0 \leq r \leq r_n} \frac{1}{M+1} \sum_{i=0}^M g(q_i) \\ &\stackrel{(c)}{=} \frac{1}{M+1} \sum_{i=0}^M g(q_i^*) := \mathbb{E}_{F_{r_n}^M}[g(P)], \end{aligned}$$

where  $q_i^* = \sigma \mathcal{Q}^{-1}\left(1 - \frac{i}{M+1}\right) + \mu(r_n)$ , for  $i \geq 1$ , and  $q_0^* = -\infty$ . (c) follows from the fact that the  $q_i$ 's are monotonically decreasing as  $r \uparrow r_n$  (because  $\mu(r)$  is a monotonically decreasing function) and that the supremum of  $g(q_i)$  is attained at  $r = r_n$  for all  $0 \leq i \leq M$  (because  $g(\cdot)$  is a monotonically decreasing function).

**Lemma 2:**  $F_{r_n}^M$  converges in distribution to  $F_{r_n}$ . That is,

$$F_{r_n}^M \xrightarrow{d} F_{r_n} \quad \text{as } M \rightarrow \infty. \quad (56)$$

*Proof:* It is easy to see that  $|F_{r_n}^M(p) - F_{r_n}(p)| \leq \frac{1}{M}$  for all  $-\infty \leq p \leq \infty$ . Therefore,  $F_{r_n}^M(p)$  converges point-wise to  $F_{r_n}(p)$ , which proves the lemma. ■

Clearly  $|g(p)| \leq 1$ . Using Lemma 2 and Theorem 19 in Chapter 7 in [60], we have  $\lim_{M \rightarrow \infty} \mathbb{E}_{F_{r_n}^M}[g(P)] = \mathbb{E}_{F_{r_n}}[g(P)]$ . From (52),  $F_{HI}^t = \mathbb{E}_{F_{r_n}}[g(P)]$ . Therefore,  $\lim_{M \rightarrow \infty} \mathbb{E}_{F_{r_n}^M}[g(P)] = F_{HI}^t$ . ■

### E. The value of improved detection algorithms

From Figure 7 we can see that even a perfect radiometer recovers only a 0.37 fraction of the weighted area for a safely low  $F_{HI}$  ( $\approx 10^{-2}$ ). It is tempting to believe that performance could be improved by considering more powerful detectors like pilot detectors and cyclostationary feature detectors [61]. It has certainly been shown that pilot detectors and cyclostationary

| <i>Research Theme</i>                        | <i>Main idea/goals</i>  | <i>References</i>     |
|--|---|-----------------------|
| Cooperation as diversity                     | Cooperation can be seen as providing diversity gains by reducing sensitivity requirements for individual radios.                  | [13], [64]            |
| Cooperation as gains in degrees of freedom   | Cooperation can be seen as reducing sensing time or lowering false alarms for the same level of detection.                        | [65], [66], [70]      |
| Impact of/Dealing with correlation           | Determining the impact of channel correlation on cooperation gains as well as mechanisms of dealing with correlation uncertainty. | [64], [69], [71]      |
| Impact of/Dealing with malicious/lying users | Determining the impact of incorrect sensing responses and mechanisms for weeding out misbehaving users.                           | [64], [72]–[74]       |
| Cooperation and Communication                | Determine the impact of communications/synchronization constraints on cooperation performance.                                    | [65], [66], [75]–[77] |
| Fusion rules                                 | Investigation of various soft/hard combining rules.   | [68], [70], [78]–[81] |
| Utilizing sparsity/multiband information     | Utilize multiple frequency bands for cooperative gains.   | [82], [83]            |

TABLE III

DESCRIPTION OF VARIOUS RESEARCH THRUSTS IN THE AREA OF COOPERATIVE SPECTRUM SENSING.

feature detectors are more robust to uncertainties in the noise process [16]. However, at best such single-user detectors can achieve the performance of a perfect radiometer, but this is limited due to the need to budget for deep fades.

## V. COOPERATION

One possible approach to solve the problem mentioned in Section IV-E is to use the sensing results from multiple nearby radios to make a decision on whether the band is free to use or not. This mirrors previous research in cooperative communications and sensor networks [62], [63]. Several groups have proposed cooperation among cognitive radios as a tool to improve performance [13], [64]–[70]. Table III lists the major research themes in the area of cooperative spectrum sensing and representative references. Gains from cooperation can either be viewed as diversity gains where multiple radios reduce the collective probability of getting a bad fade [13], [64] or as a mechanism to reduce sensing overhead [65], [66], [70]. Dealing with uncertainty (in the form of correlated data measurements and/or malfunctioning/malicious radios) forms a major component of this research. In addition, design of optimal cooperative sensing schemes under various constraints (communication/synchronization constraints for example) is also an active area of research.

We believe that the most significant gains from cooperation (from the standpoint of recovering spatial holes) are diversity gains. Hence we look at cooperation as a tool to increase WPAR. We assume that a group of  $M$  cognitive radios are listening to the primary signal on a given frequency band. This group makes a common decision on whether the band is free to use or not. For simplicity, we assume that each radio gets a perfect estimate<sup>16</sup> of the received primary power  $P_i$  (in dB)  $i = 1, \dots, M$ . We make this assumption to isolate the gains due to cooperation from those due to a longer effective sampling time.

Each of the received signal strengths is written as  $P_i = p_t - (10 \log_{10} r_i^\alpha + S_i + M_i)$ , where  $p_t$  is the transmit power of the primary signal,  $r_i$  is the distance from the  $i$ th radio to the TV tower, and  $S_i$  and  $M_i$  are respectively the losses due to shadow and multipath fading at the  $i$ th radio. All cooperating radios are assumed to be located at approximately the same distance from the TV tower, i.e.,  $r_i = r$  for all  $i = 1, 2, \dots, M$ . This models the case when the scale of cooperation is much smaller

<sup>16</sup>We can obtain a perfect received primary power estimate by running a radiometer for very long sensing times, i.e.,  $N \rightarrow \infty$ .

than the scale of the primary transmissions.<sup>17</sup> This assumption also guarantees that all the cooperating radios are trying to identify the same spectrum hole in space.

To start with, shadowing and multipath are modeled to be independent across the different radios. It is safe to assume that the  $\{M_i\}$  are independent<sup>18</sup> of each other since multipath is independent at distances on the order of a few wavelengths [84]. By contrast, shadowing is independent only on a much larger spatial scale [85]. Even though independence might not be an accurate modeling assumption, we first analyze cooperative gains under this best-case assumption. Then, Section V-D computes the loss in performance if the shadowing is not independent.

#### A. Maximum-likelihood detector: soft decision combining

Our goal is to find the optimal estimate of the distance  $r$ , given the vector of received power observations  $(P_1, P_2, \dots, P_M)$ . When the model is completely known, the optimal detector is the ML detector. We assume a nominal Gaussian model for both the shadowing and multipath distribution, i.e.,  $P_i \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(r)$  is some deterministic monotonically decreasing function of  $r$ . Under this model, the mean of the received power is dependent on its distance from the TV tower and the standard deviation is independent of the distance from the tower.

**Theorem 7:** Let  $(P_1, P_2, \dots, P_M)$  denote the vector of received power observations. Let  $P_i, i = 1, 2, \dots, M$ , be independent and identically distributed, i.e.,  $P_i \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(r)$  is some deterministic strictly monotonically decreasing function of  $r$ . Then, the maximum-likelihood estimate of the distance  $r$  given  $(P_1, P_2, \dots, P_M)$  is  $\mu^{-1}\left(\frac{1}{M} \sum_{i=1}^M P_i\right)$ . That is,

$$\arg \max_r \mathcal{P}(P_1, P_2, \dots, P_M | r_{actual} = r) = \mu^{-1}\left(\frac{1}{M} \sum_{i=1}^M P_i\right), \quad (57)$$

where  $\mu^{-1}(\cdot)$  is the inverse of the function  $\mu(\cdot)$ .

*Proof:* Under the Gaussian model,

$$\begin{aligned} \mathcal{P}(P_1, P_2, \dots, P_M | r_{actual} = r) &= \prod_{i=1}^M \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{(P_i - \mu(r))^2}{2\sigma^2}\right) \\ &= \frac{1}{(2\pi\sigma^2)^{\frac{M}{2}}} \exp\left(-\sum_{i=1}^M \frac{(P_i - \mu(r))^2}{2\sigma^2}\right) \\ \Rightarrow \arg \max_r \mathcal{P}(P_1, P_2, \dots, P_M | r_{actual} = r) &= \arg \min_r \sum_{i=1}^M \frac{(P_i - \mu(r))^2}{2\sigma^2}. \end{aligned} \quad (58)$$

Clearly, the expression on the right hand side of (58) is minimized when  $r = \mu^{-1}\left(\frac{1}{M} \sum_{i=1}^M P_i\right)$  (the second derivative of  $\sum_{i=1}^M \frac{(P_i - \mu(r))^2}{2\sigma^2}$  at  $r = \mu^{-1}\left(\frac{1}{M} \sum_{i=1}^M P_i\right)$  is greater than zero). ■

From Theorem 7, the test-statistic for the ML detector is given by  $\mu^{-1}\left(\frac{1}{M} \sum_{i=1}^M P_i\right)$ . However, since  $\mu^{-1}(\cdot)$  is a monotonic

<sup>17</sup>In reality, the radial footprint of the cooperating radios has to be dealt with as a minor increase in the no-talk radius  $r_n$ . However, we assume that the footprint of cooperation is much smaller than the margin  $(r_n - r_p)$  and thus ignore this small effect.

<sup>18</sup>This is not true strictly speaking. In general,  $M_i$ 's are conditionally independent given the shadowing environment since the shadowing environment can determine if there is or is not a strong line-of-sight path. However, we are assuming indoor operation and so there are no line-of-sight paths.

function, the ML detector is equivalent to

$$\frac{1}{M} \sum_{i=1}^M P_i \underset{D=0}{\overset{D=1}{\geq}} \lambda. \quad (59)$$

This detector computes the average received signal power on a dB scale (this is an example of a soft-decision combining rule since the radios have to send their received power values to a central combiner rather than just send 1-bit decisions) and compares it to a threshold  $\lambda$ . The frequency band is declared free if the mean signal power is less than  $\lambda$ .

**Theorem 8:** Let  $(P_1, P_2, \dots, P_M)$  denote the vector of received power observations. Assume a nominal Gaussian model for both the shadowing and multipath distribution, i.e.,  $P_i \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $\mu(r)$  is some deterministic monotonically decreasing function of  $r$ . Also, assume that the observations  $P_i$  are independent of each other. Then, the detector defined in (59) has a performance given by

$$\begin{aligned} F_{HI} &= 1 - \mathcal{Q}\left(\frac{\lambda - \mu(r_n)}{\frac{\sigma}{\sqrt{M}}}\right), \\ P_{FH}(r) &= 1 - \mathcal{Q}\left(\frac{\lambda - \mu(r)}{\frac{\sigma}{\sqrt{M}}}\right). \end{aligned} \quad (60)$$

*Proof:* By the definition for  $F_{HI}$ , we have

$$F_{HI} = \sup_{0 \leq r \leq r_n} \mathcal{P}\left(\frac{1}{M} \sum_{i=1}^M P_i < \lambda | r_{actual} = r\right). \quad (61)$$

For  $r_{actual} = r$ , we have  $P_i \sim \mathcal{N}(\mu(r), \sigma^2)$ . This implies,  $\frac{1}{M} \sum_{i=1}^M P_i \sim \mathcal{N}(\mu(r), \frac{\sigma^2}{M})$ . Using this in (61), we get

$$\begin{aligned} F_{HI} &= \sup_{0 \leq r \leq r_n} 1 - \mathcal{Q}\left(\frac{\lambda - \mu(r)}{\frac{\sigma}{\sqrt{M}}}\right) \\ &= 1 - \mathcal{Q}\left(\frac{\lambda - \mu(r_n)}{\frac{\sigma}{\sqrt{M}}}\right), \end{aligned} \quad (62)$$

where the last equality follows from the fact that  $\mu(\cdot)$  and  $\mathcal{Q}(\cdot)$  are monotonically decreasing functions.

Similarly, the probability of finding a hole is

$$\begin{aligned} P_{FH}(r) &= \mathcal{P}\left(\frac{1}{M} \sum_{i=1}^M P_i < \lambda | r_{actual} = r\right) \\ &= 1 - \mathcal{Q}\left(\frac{\lambda - \mu(r)}{\frac{\sigma}{\sqrt{M}}}\right). \end{aligned} \quad (63)$$

The WPAR can be computed by substituting (63) into (5). ■

Figure 10 shows the performance of the maximum-likelihood detector for several values of the number of cooperating radios  $M$ . It is clear that the performance significantly improves even with a few cooperating radios ( $M=5$ ). If  $M \rightarrow \infty$ , all the area is eventually recovered.

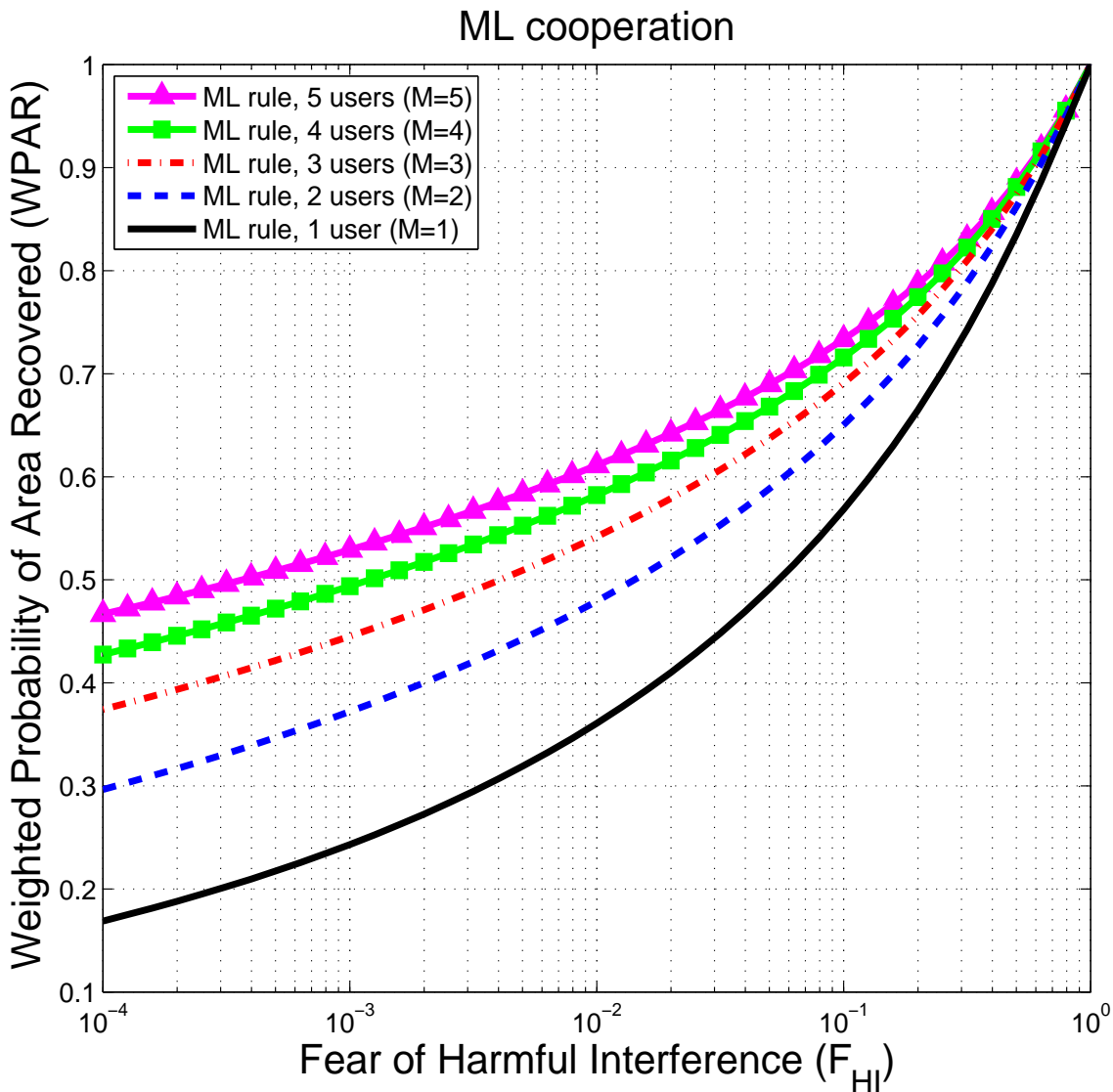


Fig. 10. Performance of the ML detector in (59) with complete knowledge of the fading/shadowing distribution.

### B. Soft-combining with uncertain models

The improvements with cooperation illustrated in Figure 10 assume complete consensus regarding the fading distribution. In reality it is likely that the primary user of the channel does not trust the nominal Gaussian models for shadowing and fading distributions. The cost of addressing this distrust of primary users is a reduced performance for the same value of safety. For now, the independence assumption for fading across different users is maintained.

Under the independent fading assumption, it is illustrative to use the quantile models discussed in Section III-D for each received power  $P_i$ . Start with a single-quantile that can be optimized. The maximum-likelihood estimate detector under uncertain fading distributions (even for a single-quantile uncertainty model) does not even make sense. Hence, we do not attempt to solve for the best possible detector under modeling uncertainties. Instead, we continue to work with the averaging detector given in (59). As discussed in Section V-A, this detector is the ML detector under perfectly modeled Gaussian fading.

**Theorem 9:** Consider  $M$  cooperating radios with  $(P_1, P_2, \dots, P_M)$  being the received power vector. Assume that  $P_i$  are

independent of each other and their marginal distributions satisfy the  $\beta$ th-quantile constraint (see Section III-D). Let the class of marginal distributions satisfying the  $\beta$ th-quantile constraint be denoted by  $\mathbb{F}_r$ . Then, for a fixed  $\beta$ , the  $F_{HI}$  for the averaging detector in (59) satisfies

$$\begin{aligned} F_{HI} &:= \sup_{0 \leq r \leq r_n} \sup_{F_r \in \mathbb{F}_r} \mathcal{P}_F \left( \frac{1}{M} \sum_{i=1}^M P_i < \lambda \mid r_{\text{actual}} = r \right) \\ &\geq 1 - (1 - \beta)^M. \end{aligned} \quad (64)$$

To compute the WPAR performance we assume nominal Gaussian models for the received powers, i.e.,  $P_i \sim \mathcal{N}(\mu(r), \sigma^2)$ , for  $i = 1, 2$ . Under this nominal model, we have

$$P_{FH}(r) = 1 - \mathcal{Q} \left( \frac{\lambda - \mu(r)}{\frac{\sigma}{\sqrt{M}}} \right), \quad \forall r \geq r_n, \quad (65)$$

and the WPAR performance is obtained by substituting (65) in (5). Furthermore, the optimal choice of  $\lambda$  that maximizes WPAR subject to the constraint that  $F_{HI} = 1 - (1 - \beta)^M$  is given by  $\lambda = \mu(r_n) + \sigma \mathcal{Q}^{-1}(1 - \beta)$ .

*Proof:* The received power vector  $(P_1, P_2, \dots, P_M)$  can be thought of as a point in  $\mathbb{R}^M$ . The equation  $\frac{1}{M} \sum_{i=1}^M P_i = \lambda$  represents an  $M - 1$  dimensional hyperplane dividing  $\mathbb{R}^M$  into two half-spaces. If the received power vector falls below the hyperplane then the detector declares the band to be empty, otherwise the band is declared as used.

Since the  $P_i$ 's are independent, every marginal distribution  $F_r \in \mathbb{F}_r$  can be mapped into a joint distribution in  $\mathbb{R}^M$ . Let  $\mathbb{F}_r^M$  denote the set of all joint distributions of  $M$  independent random variables where the marginal distribution of each random variable ( $F_r$ ) belongs to the set  $\mathbb{F}_r$ . Since each marginal distribution  $F_r \in \mathbb{F}_r$  must satisfy the  $\beta$ th-quantile constraint independently, this leads to  $2^M$  constraints on the joint distribution. We now interpret these  $2^M$  constraints geometrically. Consider the  $2^M$  regions obtained by the intersection of the  $M$  hyperplanes defined by  $P_i = \gamma(r, \beta)$ ,  $i = 1, 2, \dots, M$ , where the threshold  $\gamma(r, \beta)$  is defined in (8). Label the  $2^M$  regions by  $\mathcal{A}_j(r)$ ,  $j = 1, 2, \dots, 2^M$ . Without loss of generality we label  $\mathcal{A}_1(r) := \{(P_1, P_2, \dots, P_M) \mid (P_1 \geq \gamma(r, \beta), P_2 \geq \gamma(r, \beta), \dots, P_M \geq \gamma(r, \beta))\}$ . The  $2^M$  constraints on the joint probability distribution correspond to constraints on the probability mass in each of these regions. For instance, under the single-quantile model we know that  $\mathcal{P}(P_1 \geq \gamma(r, \beta), P_2 \geq \gamma(r, \beta), \dots, P_M \geq \gamma(r, \beta)) = \prod_{i=1}^M \mathcal{P}(P_i \geq \gamma(r, \beta)) = (1 - \beta)^M$ . This constraint can be written as  $\mathcal{P}(\mathcal{A}_1(r)) = (1 - \beta)^M =: \theta_1$ . Similarly, let  $\theta_j$ ,  $j = 1, 2, \dots, 2^M$ , denote the constraint on the probability mass allowed in region  $\mathcal{A}_j(r)$  respectively. Note that the regions  $\mathcal{A}_j(r)$  are dependent on  $r$ , whereas  $\theta_j$  are independent of  $r$ . Also,  $\sum_{j=1}^{2^M} \theta_j = 1$ .

Define,  $\mathcal{A} := \{(P_1, P_2, \dots, P_M) \in \mathbb{R}^M \mid \frac{1}{M} \sum_{i=1}^M P_i < \lambda\}$ . Then, the fear of harmful interference can be written as

$$\begin{aligned} F_{HI} &:= \sup_{0 \leq r \leq r_n} \sup_{F_r^M \in \mathbb{F}_r^M} \mathcal{P}_{F_r^M}(\mathcal{A}) \\ &\stackrel{(a)}{=} \sup_{0 \leq r \leq r_n} \sum_{j: \mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset} \theta_j. \end{aligned} \quad (66)$$

Equality (a) is true because if  $\mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset$ , then we can always choose a valid joint distribution (satisfying the single-quantile model) that places a mass of  $\theta_j$  in  $\mathcal{A}_j(r) \cap \mathcal{A}$ , and hence this probability contributes towards harmful interference.

First consider the case when  $\lambda > \gamma(r, \beta)$ . Then, clearly  $\mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset \forall j = 1, 2, \dots, 2^M$ . Therefore, we have

$$\sum_{j: \mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset} \theta_j = \sum_{j=1}^{2^M} \theta_j = 1, \quad \text{if } \lambda > \gamma(r, \beta). \quad (67)$$

Now, assume  $\lambda \leq \gamma(r, \beta)$ . Then clearly, all  $\mathcal{A}_j(r)$ ,  $j = 2, 3, \dots, 2^M$  have a non-empty intersection with  $\mathcal{A}$ , i.e.,  $\mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset$ , for all  $j = 2, 3, \dots, 2^M$ . Using this fact in (66), we get

$$\sum_{j: \mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset} \theta_j = \sum_{j=2}^{2^M} \theta_j = 1 - \theta_1 = 1 - (1 - \beta)^M, \quad \text{if } \lambda \leq \gamma(r, \beta). \quad (68)$$

Combining (67) and (68), we have

$$\sum_{j: \mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset} \theta_j = \begin{cases} 1 & \text{if } \lambda > \gamma(r, \beta) \\ 1 - (1 - \beta)^M & \text{if } \lambda \leq \gamma(r, \beta). \end{cases} \quad (69)$$

Using (69) in (66), we have

$$\begin{aligned} F_{HI} &= \sup_{0 \leq r \leq r_n} \sum_{j: \mathcal{A}_j(r) \cap \mathcal{A} \neq \emptyset} \theta_j \\ &= \sup_{0 \leq r \leq r_n} \left[ \begin{cases} 1 & \text{if } \lambda > \gamma(r, \beta) \\ 1 - (1 - \beta)^M & \text{if } \lambda \leq \gamma(r, \beta) \end{cases} \right] \\ &\stackrel{(b)}{=} \begin{cases} 1 & \text{if } \lambda > \gamma(r_n, \beta) \\ 1 - (1 - \beta)^M & \text{if } \lambda \leq \gamma(r_n, \beta), \end{cases} \end{aligned} \quad (70)$$

where (b) follows from the fact that  $\gamma(r, \beta)$  is a monotonically decreasing function. This proves the required lower bound on the fear of harmful interference.

To evaluate the WPAR, the nominal fading distribution can be assumed so we have:

$$\begin{aligned} P_{FH}(r) &= \mathcal{P} \left( \frac{1}{M} \sum_{i=1}^M P_i < \lambda | r_{actual} = r \right) \\ &= 1 - \mathcal{Q} \left( \frac{\lambda - \mu(r)}{\frac{\sigma}{\sqrt{M}}} \right). \end{aligned} \quad (71)$$

The WPAR can be computed by substituting  $P_{FH}(r)$  from (71) into (5). From (71) it is clear that  $P_{FH}(r)$  is a monotonically increasing function of  $\lambda$  for all  $r \geq r_n$ . Therefore from (70), the optimal value of  $\lambda$  such that  $F_{HI} = 1 - (1 - \beta)^M$  corresponds to  $\lambda = \gamma(r_n, \beta) = \mu(r_n) + \sigma \mathcal{Q}^{-1}(1 - \beta)$ . ■

The expression for  $F_{HI}$  in (64) for the special case of  $M = 2$  can easily be derived graphically from Figure 11. In this argument we assume that the secondary is located at the edge of the no-talk radius. In Figure 11, the  $P_1, P_2$  plane is divided into four quadrants as marked by the dashed-dotted lines (red). The single-quantile constraint on the marginal distributions can be written as probability mass constraints within each quadrant. The averaging detector in (59) for a fixed  $\lambda$  can be drawn as a straight line dividing the  $P_1, P_2$  plane into two half planes (the solid (blue) line in Figure 11). If the received power ( $P_1, P_2$ )

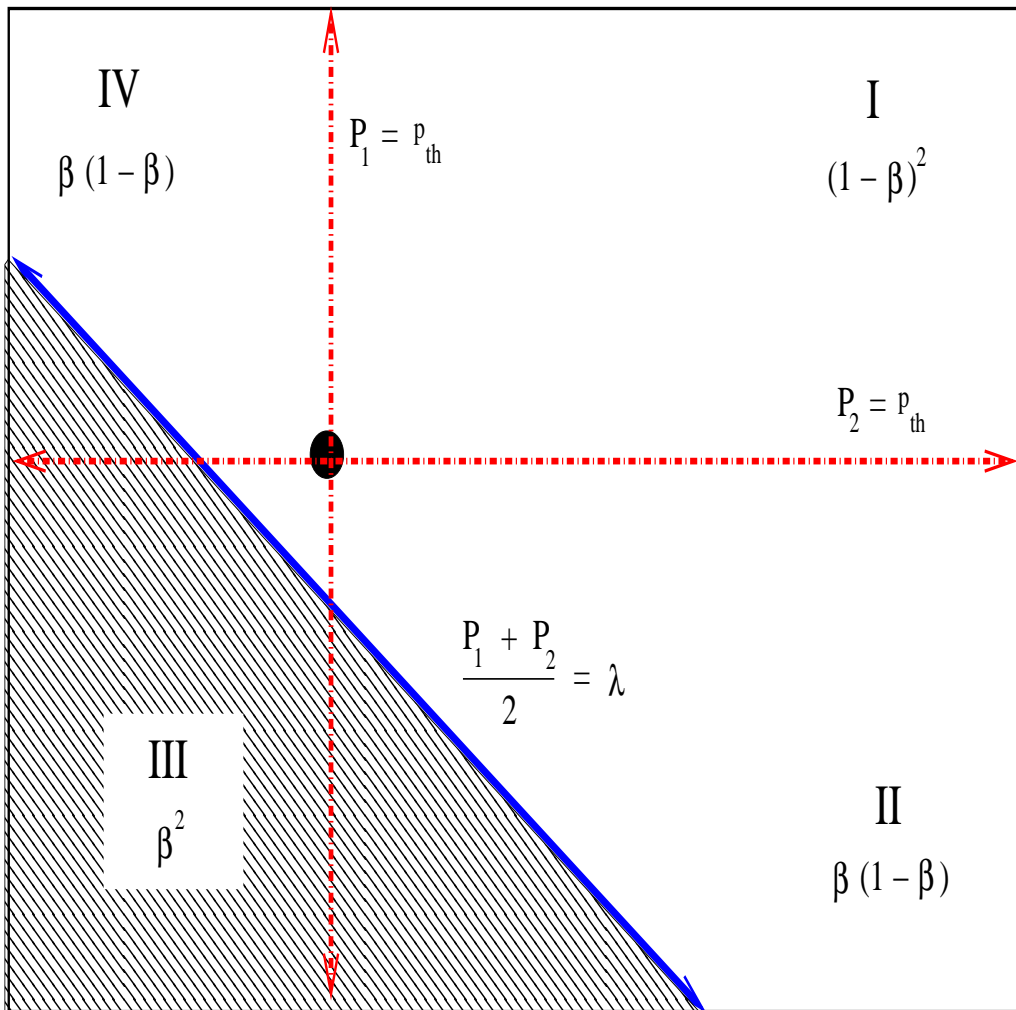


Fig. 11. The averaging detector for two user cooperation under the single-quantile fading model. The solid (black) box in the perimeter represents the  $P_1$ ,  $P_2$  plane, the solid (blue) line represents the 2-user ML detector in (59), and the dashed (red) lines represent the quantiles describing the distribution of  $P_1$  and  $P_2$ . The shaded area represents the region of the received power pairs  $(P_1, P_2)$  for which the detector declares the band unused and the unshaded area represents the region where the detector declares the band as used. The threshold  $p_{th}$  in the figure is used to denote  $\gamma(r_n, \beta)$ .

falls in the shaded region, the band is declared ‘free to use’, otherwise the band is declared ‘used’. Hence, the probability of harmful interference is the supremum of the probability mass in the shaded region, where the supremum is taken over all distributions  $F \in \mathbb{F}_\beta$ . Similarly, the probability of finding a hole is the probability mass in the unshaded region, under the nominal distribution.

If  $\lambda \leq \gamma(r_n, \beta)$  (the detector line is on the left of the black dot in the figure), then  $F_{HI}$  is the sum of probabilities in quadrants II, III, and IV. This is because one can always choose a distribution that satisfies the quantile constraints and puts all the probability mass in quadrants II, III, and IV within the shaded region. Thus, in this case  $F_{HI} = 1 - (1 - \beta)^2$ . On the other hand if  $\lambda > \gamma(r, \beta)$ , then  $F_{HI} = 1$ . Therefore, the optimal choice of  $\lambda$  for a given quantile  $\beta$  that minimizes  $F_{HI}$  and maximizes  $WPAR$  is  $\lambda = \gamma(r_n, \beta)$ .

Figure 12 plots the performance of the averaging detector under the single-quantile model for the fading distribution. The dashed curve (blue) is the performance of the averaging detector when the fading distribution is completely known (in this case the averaging detector is the ML detector). The solid curve (black) is the performance of the averaging detector under



minimal knowledge of the fading distribution, i.e., with knowledge of a single-quantile. From the figure it is clear that the 2-user averaging detector is highly non-robust to uncertainties in the fading distribution. This shows that blindly using the form of the ML detector (averaging) assuming complete knowledge can be disastrous under modeling uncertainties.

The performance of the averaging detector improves if we assume multiple quantile knowledge for shadowing and fading distributions. The mathematical analysis of multiple quantiles is similar to that of the single-quantile model and is omitted here. The performance is shown in Figure 13 and it is clear that the performance of the averaging detector improves as we learn more quantiles about the fading distribution. However, the first few quantiles learned give more performance improvement than the later ones — with performance approaching that of a fully trusted nominal model as the number of trusted quantiles increases.

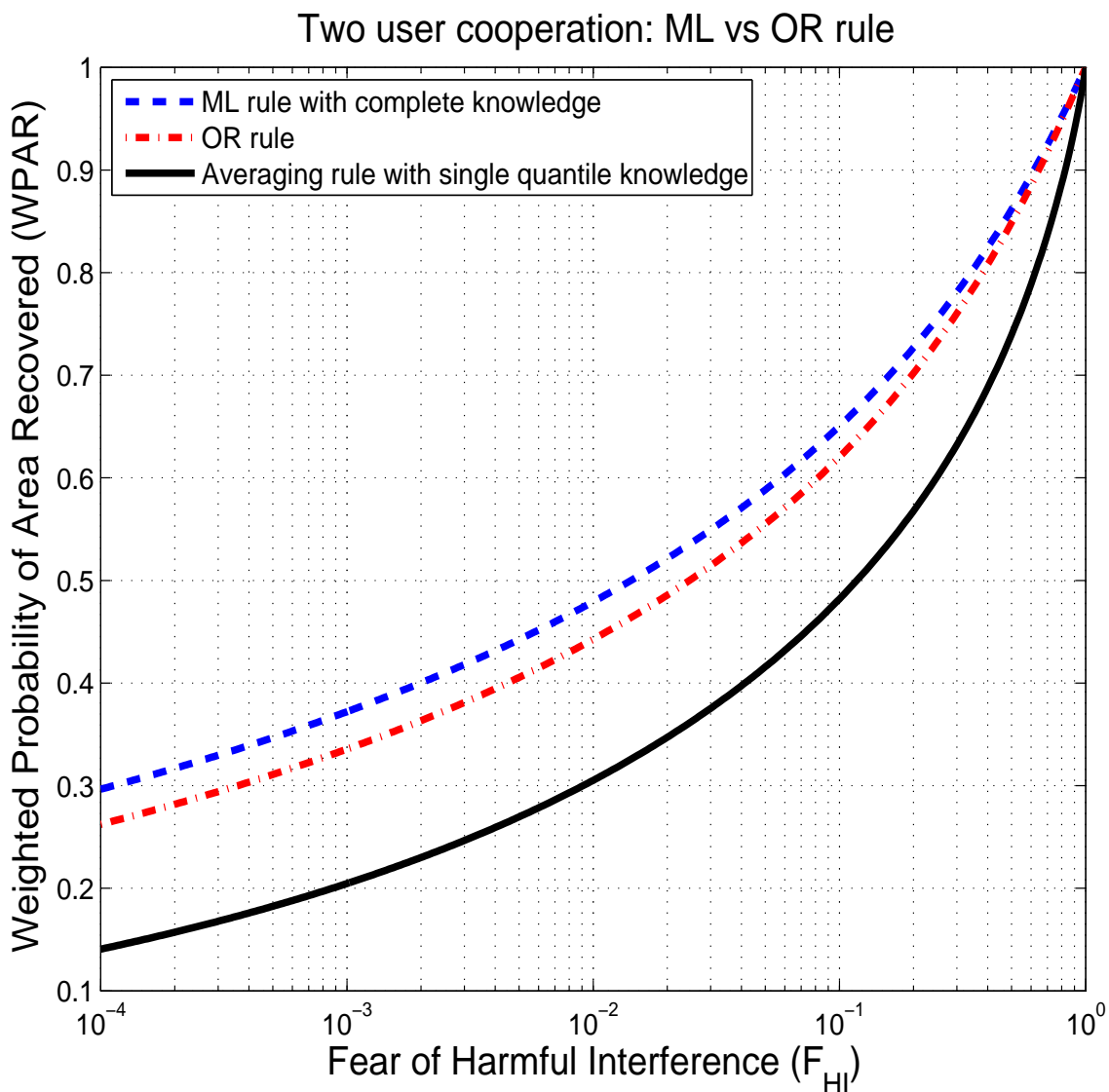


Fig. 12. Averaging detector for two user cooperation: performance under complete knowledge of the fading/shadowing distribution versus performance under the single-quantile uncertainty model for fading/shadowing distribution.

Figure 14 shows the performance of the averaging detector under the single-quantile model for  $M \geq 2$ , with  $F_{HI} = 10^{-2}$ .

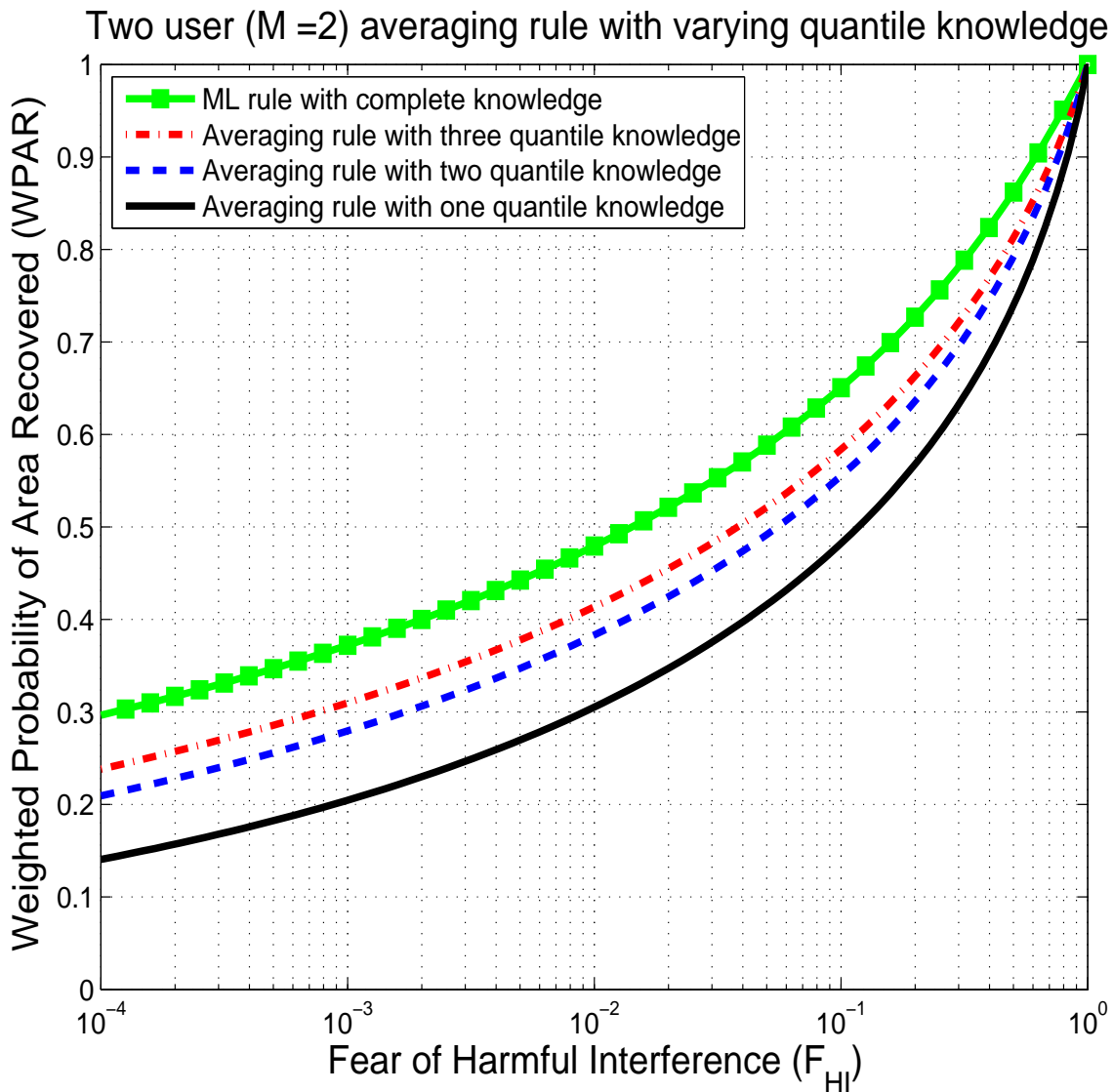


Fig. 13. Performance of the averaging detector under varying quantile knowledge for the shadowing and fading distributions. The quantiles were chosen to minimize  $F_{HI}$  for a given WPAR value.

The solid curve is the averaging detector with single-quantile knowledge, the dashed-dotted curve is the ‘OR-rule’ detector (discussed in the next section) and the dashed curve is the averaging detector with complete trust in the nominal distributional (in this case the averaging detector is the ML detector). Note that whereas the performances of the OR rule and the averaging detector under complete distributional knowledge improve with increasing  $M$ , the averaging detector with single-quantile knowledge does worse as the number of cooperating radios  $M$  increases! This is because the number of quantiles contributing towards  $F_{HI}$  increases exponentially with the number of users.<sup>19</sup> This shows the non-robustness of blindly using the form of the ML detector even under uncertainties.

<sup>19</sup>To understand why the averaging detector is so vulnerable to uncertainties of this form, remember that the empirical average is very sensitive to outliers. A single very negative number can dominate the entire average. Quantile models can be thought of as histograms. As such, they do not impose any restriction on how negative the rare bad fading can be since the outermost bin of a histogram includes everything from  $-\infty$  on up. Consequently, the averaging detector cannot afford even a single user experiencing a fade from that lowermost bin.

### C. OR rule detector: hard decision combining

We now explore a more robust detection algorithm which performs well even under minimal models for the fading distribution – the “OR-rule combining” [64]. This is a hard-decision combining strategy where each radio compares its received power to a threshold. It tentatively declares the band free to use if its received power is below the threshold. Then, each radio sends its tentative 1-bit sensing decision to the central combiner (there are other ways to fuse decision based on the radio topology [86]). The global decision is to use the band only if all the sensors declare the band to be free. Mathematically, this hard-decision combining strategy is described below.

**Definition 5:** The “OR rule” detector performs the following operations:

- 1) Each radio computes its received power  $P_i$ ,  $i = 1, 2, \dots, M$ .
- 2) The radios compare the received powers  $P_i$  to a threshold,  $\lambda_{radio,M}$ . They tentatively declare the band free to use if its received power is below the threshold, i.e.,

$$P_i \underset{D_i=0}{\overset{D_i=1}{\geq}} \lambda_{radio,M}.$$

- 3) Then, each radio sends its tentative 1-bit sensing decision ( $D_i$ ) to the central combiner.
- 4) The central combiner makes the global decision to use the band only if all the sensors declare the band to be free, i.e., the global decision is given by  $D^c = \prod_{i=1}^M D_i^c$ , where  $D^c$  denotes the complement of the binary variable  $D$ .

**Theorem 10:** Let  $(P_1, P_2, \dots, P_M)$  denote the vector of received power observations. Assume that the observations  $P_i$  are *iid* and their marginal distribution  $F_r$  lies in the class of distributions  $\mathbb{F}_r$  satisfying the single-quantile model in Definition 4. Set  $\gamma(r_n, \beta) := \lambda_{radio,M}$ , which in turn implies  $\beta = 1 - \mathcal{Q}\left(\frac{\lambda_{radio,M} - \mu(r_n)}{\sigma}\right)$ , where  $\lambda_{radio,M}$  is the detector threshold for the individual radio with  $M$  cooperating radios (see Definition 5). Then, the safety/performance of the OR-rule detector described in Definition 5 is given by

$$\begin{aligned} F_{HI,system} &= \left[ 1 - \mathcal{Q}\left(\frac{\lambda_{radio,M} - \mu(r_n)}{\sigma}\right) \right]^M, \\ P_{FH,system}(r) &= \left[ 1 - \mathcal{Q}\left(\frac{\lambda_{radio,M} - \mu(r)}{\sigma}\right) \right]^M. \end{aligned} \quad (72)$$

Substituting (72) in (5), we get the WPAR for the OR rule. Furthermore, if we require  $F_{HI,system} \leq F_{HI}^{target}$ , then the optimal choice of  $\lambda_{radio,M}$  is given by

$$\lambda_{radio,M} = \sigma \mathcal{Q}^{-1}\left(1 - [F_{HI}^{target}]^{\frac{1}{M}}\right) + \mu(r_n). \quad (73)$$

*Proof:* It is easy to see that the fear of harmful interference for the OR rule is maximized at the edge of the no-talk radius. So, we focus our attention to the case when all the  $M$  cooperating radios are located at the edge of the no-talk radius.

Define  $F_{HI,radio} := 1 - \mathcal{Q}\left(\frac{\lambda_{radio,M} - \mu(r_n)}{\sigma}\right)$ .  $F_{HI,radio}$  is the worst-case probability (under the set of uncertain distributions  $\mathbb{F}_{r_n}$ ) that a single-radio located at the edge of the no-talk radius will fail to trigger the threshold  $\lambda_{radio,M}$ . This is true because the threshold in the single-quantile model is matched to the detection threshold, i.e.,  $\gamma(r_n, \beta) = \lambda_{radio,M}$  (see Equation (28)).

Now, under the OR-rule, the system of cognitive radios causes harmful interference only if every radio individually fails to

detect the primary, and so by independence:

$$\begin{aligned} F_{HI,system} &= F_{HI,radio}^M \\ &= \left[ 1 - \mathcal{Q} \left( \frac{\lambda_{radio,M} - \mu(r_n)}{\sigma} \right) \right]^M. \end{aligned} \quad (74)$$

From (74) it clear that for  $F_{HI,system} = F_{HI}^{target}$ , we must have

$$\begin{aligned} \mathcal{Q} \left( \frac{\lambda_{radio,M} - \mu(r_n)}{\sigma} \right) &= 1 - [F_{HI}^{target}]^{\frac{1}{M}} \\ \Rightarrow \lambda_{radio,M} &= \sigma \mathcal{Q}^{-1} \left( 1 - [F_{HI}^{target}]^{\frac{1}{M}} \right) + \mu(r_n). \end{aligned} \quad (75)$$

As  $M \rightarrow \infty$ , it is immediately clear that for any given target  $F_{HI}$ , the term  $[F_{HI}^{target}]^{\frac{1}{M}} \rightarrow 1$  and so the threshold (and thus target quantile) approaches the case of extremely favorable fading.

For such a choice of  $\lambda_{radio,M}$ , the probability of finding a hole at a radial distance of  $r$  is given by

$$\begin{aligned} P_{FH,radio}(r) &= \mathcal{P}(P_i < \lambda_{radio,M} | r_{actual} = r) \\ &= 1 - \mathcal{Q} \left( \frac{\lambda_{radio,M} - \mu(r)}{\sigma} \right). \end{aligned}$$

The system finds a hole only if all the radios find a hole. Therefore,

$$\begin{aligned} P_{FH,system}(r) &= (P_{FH,radio})^M \\ &= \left[ 1 - \mathcal{Q} \left( \frac{\lambda_{radio,M} - \mu(r)}{\sigma} \right) \right]^M. \end{aligned} \quad (76)$$

■

It is clear from substituting (75) into (76) that under the single-quantile model of uncertainty and nominal Gaussian fading, the WPAR tends to 1 for the OR rule as the number of cooperating users increases. Figure 12 compares the performance of the OR-rule detector with the averaging detector with complete knowledge, and the averaging detector with single-quantile knowledge for the case of two cooperating radios ( $M = 2$ ) while Figure 14 compares the same for the case of  $M > 2$ . It is clear that the OR rule is much more robust to uncertainty in the fading distribution than the averaging rule.

Gains by using the OR rule are accomplished by taking the single quantile to correspond to ever more favorable fading realizations. This is problematic since it involves achieving a consensus regarding the rare best fading events — this is as implausible as achieving a consensus regarding the rare worst-fading events. In addition, there is a very natural deployment scenario — outdoors on a rooftop — in which the best fading events cannot be too good. This is a little counterintuitive, but remember that multipath fading can result in both destructive and constructive interference. Indoors or in an urban canyon, the best-case fading corresponds to lucky constructive interference. Outdoors, with a dominant line-of-sight path, such constructive interference cannot occur.

Strangely enough, when cooperation is involved, it is this possibility of a clean line-of-sight path that requires the uncertainty

model  $\mathbb{F}_r$  to impose a bound on how lucky the fading can be. This effectively caps  $\lambda_{radio,M}$  to the fade that corresponds to a single line-of-sight path. Once the number of cooperating users has reached a point that they can support the desired  $F_{HI}$  using that particular quantile, there is no further benefit to increasing the number of users if the OR rule is used. In fact, the performance will drop if cooperating users are blindly added as there is an increased chance of a single user (who happens to be in a rich multipath environment) getting a very lucky constructive fade and thereby deciding that they are within the no-talk radius. The kinked-green curve in Figure 14 illustrates what happens if the uncertain fading model includes the possibility for a line-of-sight path at the 10%-best quantile.

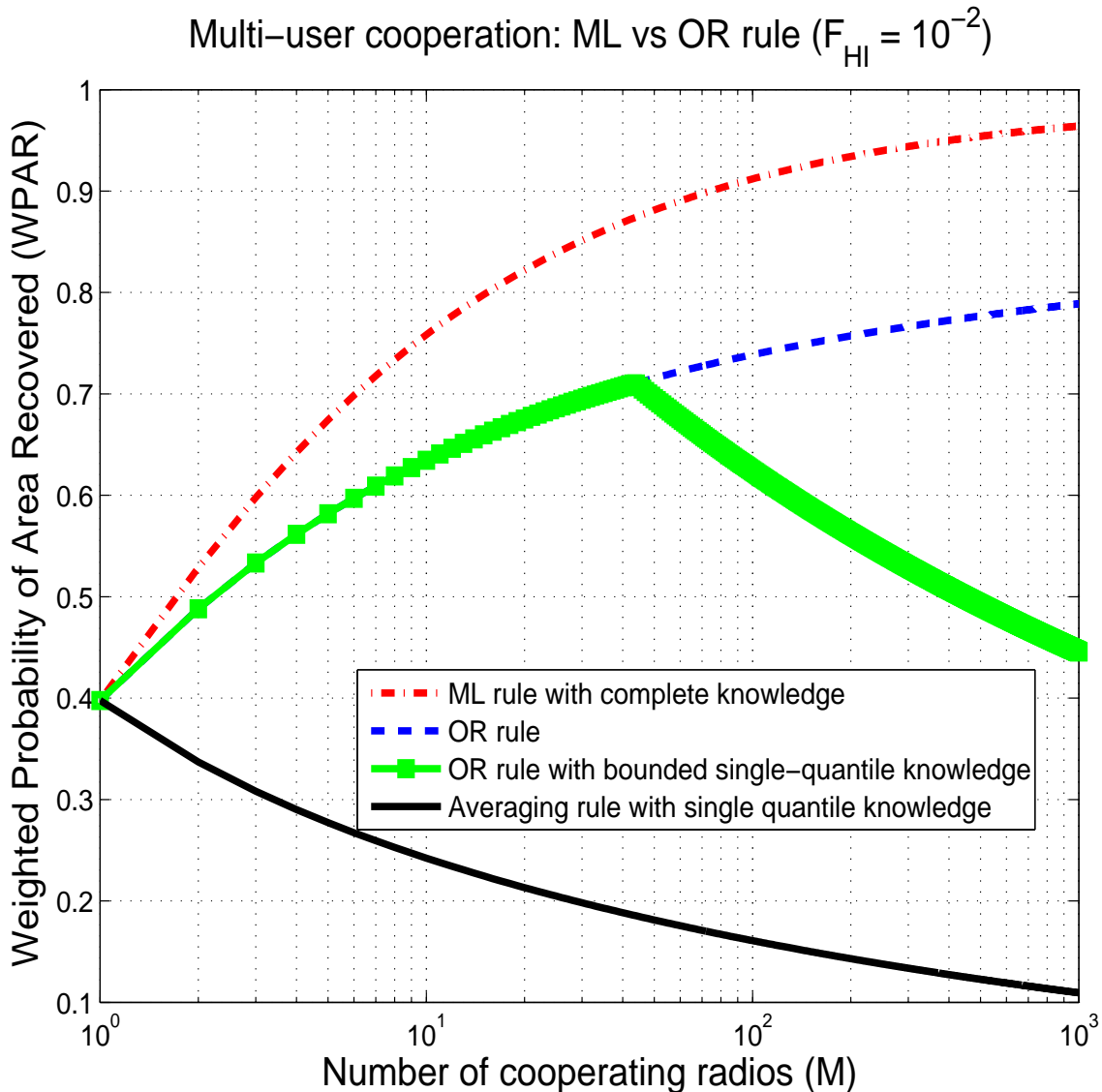


Fig. 14. Performance of detectors as a function of the number of cooperating users  $M$  for a fixed target  $F_{HI} = 10^{-2}$ .

Other weighted-percentage rules for hard-decision combining have also been proposed and these are a little more tolerant of modeling inaccuracies [64] in general. In particular, such rules are going to be required to avoid the performance penalty that arises from the fear of line-of-sight, but we do not dwell into the details of such rules in this technical report.

#### D. Performance of cooperation under loss of independence

We have shown that safety/performance can improve significantly if radios cooperatively sense for the primary user as compared to sensing individually. This assumed that the channels from the primary transmitter to the individual secondary radios are independent. However, the primary user might not trust this assumption since all the cognitive radios may be behind the same obstacle and hence see correlated shadowing. We show that this implies that the detector needs to set its thresholds conservatively, leading to a loss in WPAR performance. The issue of correlated-shadowing was also discussed in [71], where the authors examine the performance of their proposed linear-quadratic detector with correlation uncertainty. The proposed detector is shown to have better probability of detection than a simple counting rule for correlation values greater than 0.4.

As before, let  $(P_1, P_2, \dots, P_M)$  be the received powers at the  $M$  secondary users. To isolate the effect of dependent shadowing, we assume that the marginal distributions for  $P_i$  are completely known, but there is some uncertainty in the correlation across users.

**Theorem 11:** Let  $(P_1, P_2, \dots, P_M)$  denote the vector of received power observations. Assume that  $(P_1, P_2, \dots, P_M)$  is a jointly Gaussian random vector with marginals given by  $P_i \sim \mathcal{N}(\mu(r), \sigma^2)$ , where  $r$  is the common radial distance from the primary transmitter. Assume that the  $M \times M$  covariance matrix  $C$  for the random vector  $(P_1, P_2, \dots, P_M)$  has entries  $C(i, j)$  given by

$$C(i, j) = \begin{cases} \rho\sigma^2 & \text{if } i \neq j \\ \sigma^2 & \text{if } i = j, \end{cases}$$

where the correlation coefficient  $\rho$  is uncertain within known bounds, i.e.,  $\rho \in [0, \rho_{max}]$ , with  $0 \leq \rho_{max} \leq 1$ . Let  $\rho = 0$  (complete independence among the cooperating radios) correspond to the nominal model used for computing the WPAR performance.

Then, the safety/performance of the averaging detector in (59) is given by

$$\begin{aligned} F_{HI} &= \sup_{0 \leq \rho \leq \rho_{max}} \left[ 1 - \mathcal{Q} \left( \frac{\lambda - \mu(r_n)}{\sqrt{\frac{1}{M}[1 + (M-1)\rho]\sigma^2}} \right) \right], \\ P_{FH}(r) &= 1 - \mathcal{Q} \left( \frac{\lambda - \mu(r)}{\frac{\sigma}{\sqrt{M}}} \right), \end{aligned} \quad (77)$$

where  $\lambda$  is the averaging detector threshold. Furthermore, for a low safety constraint, i.e.,  $F_{HI} \leq F_{HI}^{target} \leq 0.5$ , the averaging detector must design its  $\lambda$  for the worst-case correlation,  $\rho = \rho_{max}$ . That is, the supremum in (77) is attained for  $\rho = \rho_{max}$ .

*Proof:* The test-statistic for the averaging detector is  $\frac{1}{M} \sum_{i=1}^M P_i \sim \mathcal{N}(\mu(r), \frac{1}{M}[1 + (M-1)\rho]\sigma^2)$ . Therefore,

$$\begin{aligned} F_{HI} &= \sup_{0 \leq \rho \leq \rho_{max}} \mathcal{P} \left( \frac{1}{M} \sum_{i=1}^M P_i < \lambda | r_{actual} = r_n \right) \\ &= \sup_{0 \leq \rho \leq \rho_{max}} \left[ 1 - \mathcal{Q} \left( \frac{\lambda - \mu(r_n)}{\sqrt{\frac{1}{M}[1 + (M-1)\rho]\sigma^2}} \right) \right]. \end{aligned} \quad (78)$$

Similarly, under the nominal model  $\frac{1}{M} \sum_{i=1}^M P_i \sim \mathcal{N}(\mu(r), \frac{\sigma}{\sqrt{M}})$ . Therefore,

$$\begin{aligned} P_{FH}(r) &= \mathcal{P} \left( \frac{1}{M} \sum_{i=1}^M P_i < \lambda | r_{actual} = r \right) \\ &= 1 - \mathcal{Q} \left( \frac{\lambda - \mu(r)}{\frac{\sigma}{\sqrt{M}}} \right). \end{aligned} \quad (79)$$

Now, for a given  $F_{HI}^{target} \leq 0.5$  we must choose  $\lambda$  such that

$$\begin{aligned} F_{HI}^{target} &= \sup_{0 \leq \rho \leq \rho_{max}} \left[ 1 - \mathcal{Q} \left( \frac{\lambda - \mu(r_n)}{\sqrt{\frac{1}{M}[1 + (M-1)\rho]\sigma^2}} \right) \right] \\ \Rightarrow 1 - F_{HI}^{target} &= \inf_{0 \leq \rho \leq \rho_{max}} \mathcal{Q} \left( \frac{\lambda - \mu(r_n)}{\sqrt{\frac{1}{M}[1 + (M-1)\rho]\sigma^2}} \right) \\ \Rightarrow 1 - F_{HI}^{target} &= \mathcal{Q} \left( \sup_{0 \leq \rho \leq \rho_{max}} \left[ \frac{\lambda - \mu(r_n)}{\sqrt{\frac{1}{M}[1 + (M-1)\rho]\sigma^2}} \right] \right). \end{aligned} \quad (80)$$

The last equality follows from the fact that  $\mathcal{Q}(\cdot)$  is a monotonically decreasing function. Now,  $F_{HI}^{target} \leq 0.5$  implies  $1 - F_{HI}^{target} \geq 0.5$ . Therefore,  $\lambda \leq \mu(r_n)$  in (80). This implies,

$$\begin{aligned} \sup_{0 \leq \rho \leq \rho_{max}} \left[ \frac{\lambda - \mu(r_n)}{\sqrt{\frac{1}{M}[1 + (M-1)\rho]\sigma^2}} \right] &= \frac{\lambda - \mu(r_n)}{\sup_{0 \leq \rho \leq \rho_{max}} \left[ \sqrt{\frac{1}{M}[1 + (M-1)\rho]\sigma^2} \right]} \\ &= \frac{\lambda - \mu(r_n)}{\sqrt{\frac{1}{M}[1 + (M-1)\rho_{max}]\sigma^2}}. \end{aligned}$$

Substituting this in (80) gives us the desired result. ■

Figure 15 shows the performance of the averaging detector designed for different values of  $\rho_{max}$ . It is clear that as the amount of uncertainty in the correlation increases, the performance of the averaging detector decreases. Even a small amount of correlation results in a significant drop in performance. As the number of users increases, this particular model of correlation is even more harmful. This can be seen by giving a simple interpretation to this correlation – fading for any user is the sum of a common random fading and a fade local to this user. It is clear that no amount of cooperation can overcome the non-spatially-ergodic common fade. Without a way to combat the fear of such non-spatially-ergodic shadowing uncertainty, there is no way to safely recover the full spectrum hole.

## VI. CALIBRATION AND ASSISTED DETECTION

Section IV analyzed the issues with a single radio trying to achieve a very low  $F_{HI}$ . Such a detector must budget for the worst-case multipath and shadowing and hence loses significant area when the channel is not badly shadowed. The previous section argued that cooperation among independently shadowed users can help, but offered no hope for the physically important case of users that might experience common shadowing. For example, the uncertainty in the deployment scenario of indoor vs outdoor use can easily manifest as users that are all indoors (and thus shadowed) or outdoors.

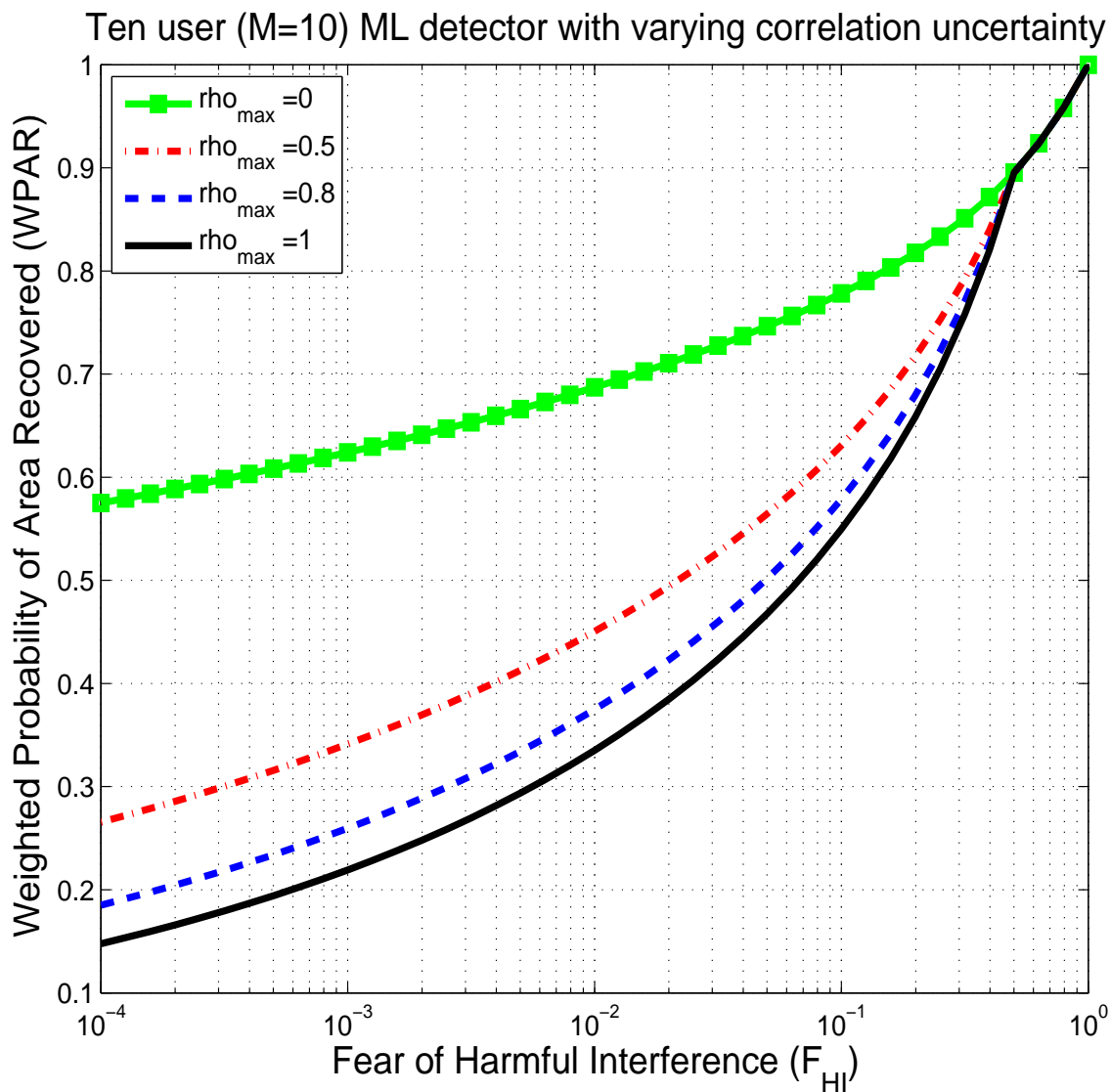


Fig. 15. Performance of the averaging detector with varying amount of correlation uncertainty,  $\rho_{max}$ . These plots correspond to the case of ten cooperating users, i.e.,  $M = 10$ .

If such a radio had information about its shadowing environment it could budget for the actual shadowing and thus improve on its probability of finding a spectrum hole without giving up any safety. A detection mechanism where side information is used to aid the detector is called calibrated or assisted detection. One example of assisted detection in the cognitive-radio context is interference calibration. If interference from other radios extends beyond a single primary frequency band, then adjacent bands can be used to estimate the interference level and improve the robustness of the detector [16]. Another such example is assisted GPS, where a GPS receiver obtains side information from TV/cell-towers to reduce its uncertainty about its location, time, etc [87], [88]. This section shows how assisted detection improves the  $F_{HI}/WPAR$  performance of a single-radio spectrum sensor.



### A. Satellite bands as a calibration mechanism

One of the advantages of satellites is that the path loss from a satellite is constant to all places within a large area (for example the San Francisco Bay Area). Hence the signal strength of satellite can be deterministically subtracted to reveal the shadowing + multipath component. So how is satellite shadowing in a separate frequency band related to shadowing from a TV tower in the band of interest? Consider two hypothetical radios: one on the roof of a building and the other in the basement. The radio in the basement will see both the satellite and TV signals at low power levels as compared to the radio on the roof. This suggests that shadowing can be broken up into a directional component that depends on the location of the transmitter and a portion that is direction agnostic. Furthermore, the direction-agnostic shadowing is also wideband – it remains the same across frequencies [82].

### B. Satellite-assisted detector

In this section we evaluate potential gains from using satellite-assisted detection, under a very simple model. We assume that the secondary radio gets perfect estimates of the received signal strengths in the primary and satellite bands. Let  $(P_1, P_2)$  denote the received power (in dBm) from the primary and satellite bands respectively. We model

$$\begin{aligned} P_1 &= p_t - (10 \log_{10}(r^\alpha) + S_1), \\ P_2 &= p_g - (L_g + S_2), \end{aligned} \quad (81)$$

where  $p_g$  is the transmit power of the satellite signal, and  $L_g$  is the path loss from the satellite transmitter to any radio in this given geographic area. As the distance from the satellite transmitter to any receiver is approximately constant, we assume that  $L_g$  is a known deterministic constant.  $S_1$  is the loss due to shadowing and multipath fading encountered by the primary, i.e.,  $S_1 = S + M_1$ . Similarly,  $S_2$  is the loss encountered by the satellite signal due to fading and can be written as  $S_2 = S + M_2$ . We conjecture that the shadowing in the satellite band and the TV band are highly correlated and for simplicity, they are modeled as being identical.  $M_1, M_2$  are *i.i.d.* multipath random variables for the TV and satellite bands. From (81) it is clear that having access to  $(P_1, P_2)$  is equivalent to having access to  $(P_1, S_2)$ . This is because  $p_g$  and  $L_g$  are known constants. Therefore, we can safely assume that the secondary radio get a perfect estimate of  $(P_1, S_2)$ .

**Theorem 12:** Let  $P_1$  be the received power from the primary and let  $S_2$  denote the shadowing in the satellite band to the secondary. Further, let  $(P_1, S_2)$  be jointly Gaussian random variables with statistics given by

$$\begin{bmatrix} P_1 \\ S_2 \end{bmatrix} \sim \mathcal{N} \left( \begin{bmatrix} \mu(r) \\ \mu_2 \end{bmatrix}, \begin{bmatrix} \sigma_1^2 & -\rho \sigma_1 \sigma_2 \\ -\rho \sigma_1 \sigma_2 & \sigma_2^2 \end{bmatrix} \right), \quad (82)$$

where  $\mu(r)$  is a known monotonically decreasing function of the distance from the primary transmitter ( $r$ ), and  $(\rho, \mu_2, \sigma_1, \sigma_2)$  are known constants. Then, the maximum-likelihood estimate of the distance  $r$  given  $(P_1, S_2)$  is  $\mu^{-1} \left( P_1 + \rho \frac{\sigma_1}{\sigma_2} (S_2 - \mu_2) \right)$ .

That is,

$$\arg \max_r \mathcal{P}(P_1, S_2 | r_{actual} = r) = \mu^{-1} \left( P_1 + \rho \frac{\sigma_1}{\sigma_2} (S_2 - \mu_2) \right), \quad (83)$$

where  $\mu^{-1}(\cdot)$  is the inverse of the function  $\mu(\cdot)$ .

*Proof:* Under the Gaussian model the ML estimate of  $\mu(r)$  is the value of  $\mu(r)$  that minimizes,

$$F = [P_1 - \mu(r) \ S_2 - \mu_2] \begin{bmatrix} \sigma_1^2 & -\rho \sigma_1 \sigma_2 \\ -\rho \sigma_1 \sigma_2 & \sigma_2^2 \end{bmatrix}^{-1} [P_1 - \mu(r) \ S_2 - \mu_2]^T. \quad (84)$$

The above is a quadratic in  $\mu(r)$  and the minimizing value can be obtained by setting  $\frac{dF}{d\mu(r)} = 0$ .

$$\frac{dF}{d\mu(r)} = \frac{2}{\sigma_1^2(1-\rho^2)}(-P_1 + \mu(r)) - \frac{2\rho}{(1-\rho^2)\sigma_1\sigma_2}(S_2 - \mu_2). \quad (85)$$

Setting  $\frac{dF}{d\mu(r)} = 0$ , we get the ML estimate of  $\mu(r)$  to be  $P_1 + \frac{\rho\sigma_1}{\sigma_2}(S_2 - \mu_2)$ . Hence the ML estimate of  $r$  given  $(P_1, S_2)$  is  $\mu^{-1}\left(P_1 + \frac{\rho\sigma_1}{\sigma_2}(S_2 - \mu_2)\right)$ . ■

From Theorem 12, the test-statistic of the ML detector for satellite-assisted detection is given by  $\mu^{-1}\left(P_1 + \frac{\rho\sigma_1}{\sigma_2}(S_2 - \mu_2)\right)$ . However, since  $\mu^{-1}(\cdot)$  is a monotonic function, the ML detector is equivalent to

$$T(P_1, S_2) := P_1 + \frac{\rho\sigma_1}{\sigma_2} S_2 \underset{D=0}{\overset{D=1}{\gtrless}} \lambda. \quad (86)$$

**Theorem 13:** Let  $P_1$  be the received primary power at the secondary radio, and  $S_2$  denote the shadowing in the satellite band to the secondary radio. Assume  $(P_1, S_2)$  are jointly Gaussian random variables satisfying

$$\begin{bmatrix} P_1 \\ S_2 \end{bmatrix} \sim \mathcal{N} \left( \begin{bmatrix} \mu(r) \\ \mu_2 \end{bmatrix}, \begin{bmatrix} \sigma_1^2 & -\rho \sigma_1 \sigma_2 \\ -\rho \sigma_1 \sigma_2 & \sigma_2^2 \end{bmatrix} \right), \quad (87)$$

where  $\mu(r)$  is a known monotonically decreasing function of the distance from the primary transmitter  $r$ , and  $(\rho, \mu_2, \sigma_1, \sigma_2)$  are known constants.

Then, the safety/performance of the weighted-average detector given in (86) is

$$\begin{aligned} F_{HI} &= 1 - Q \left( \frac{\lambda - (\mu(r_n) + \rho \frac{\sigma_1}{\sigma_2} \mu_2)}{\sigma_1 \sqrt{1 - \rho^2}} \right), \\ P_{FH}(r) &= 1 - Q \left( \frac{\lambda - (\mu(r) + \rho \frac{\sigma_1}{\sigma_2} \mu_2)}{\sigma_1 \sqrt{1 - \rho^2}} \right). \end{aligned} \quad (88)$$

*Proof:* Under the jointly Gaussian model in (87), the distribution of the test statistic  $T(P_1, S_2)$  at a distance  $r$  is given by:

$$T(P_1, S_2) \sim \mathcal{N} \left( \mu(r) + \rho \frac{\sigma_1}{\sigma_2} \mu_2, \sigma_1(1 - \rho^2) \right). \quad (89)$$

Hence, the fear of harmful interference is

$$\begin{aligned}
F_{HI} &= \sup_{0 \leq r \leq r_n} \mathcal{P}(T(P_1, S_2) < \lambda | r_{actual} = r) \\
&\stackrel{(a)}{=} \mathcal{P}(T(P_1, S_2) < \lambda | r_{actual} = r_n) \\
&= 1 - Q\left(\frac{\lambda - (\mu(r_n) + \rho \frac{\sigma_1}{\sigma_2} \mu_2)}{\sigma_1 \sqrt{1 - \rho^2}}\right).
\end{aligned} \tag{90}$$

Here, (a) is true because a secondary radio at the edge of the no-talk radius is the worst-case scenario. This can be mathematically shown by using the fact that  $\mu(r)$  is monotonically decreasing in  $r$  and  $Q(\cdot)$  is also monotonically decreasing.

Similarly,  $P_{FH}(r)$  is given by:

$$\begin{aligned}
P_{FH}(r) &= \mathcal{P}_{F_r}(T(P_1, S_2) < \lambda) | r_{actual} = r) \\
&= 1 - Q\left(\frac{\lambda - (\mu(r) + \rho \frac{\sigma_1}{\sigma_2} \mu_2)}{\sigma_1 \sqrt{1 - \rho^2}}\right).
\end{aligned} \tag{91}$$

■

The performance of this detector compared to a single radio is shown in Figure 16. From the figure, it is evident that the performance improves as the level of correlation between the satellite-band fading and TV-tower fading increases. This corresponds to when both the signals are wideband and so multipath is relatively less significant. In the extreme of no-multipath ( $\rho = 1$ ), all the area can be recovered by a single satellite-assisted spectrum sensor.

If the number of cooperating sensors is increased and the non-common shadowing were guaranteed to be independent across sensors, then satellite-assisted techniques can completely overcome the deployment uncertainty that otherwise manifests as correlated shadowing across users. This is best understood by interpreting the correlation among radios in Figure 15 as a result of the shadowing term that is common to all radios i.e. received power at radio  $i$  can be written as  $P_i = p_t - (l(r) + S + M_i)$  where  $S$  is the common shadowing term and  $M_i$  are the independent multipath terms. If measurements in the satellite band can help us completely resolve the value of  $S$  then increasing the number of radios can help us eliminate the effect of the independent multipath and hence recover all area (this is best seen by examining Equation (63) for uncorrelated radios. For  $F_{HI} < 0.5$ ,  $\lambda$  will be greater than  $\mu(r)$  for all values of  $r$  and hence increasing  $M$  will cause  $P_{FH}(r)$  to go to 1 for all values of  $r$ ).

### C. Performance of assisted detection with quantile models

The ML detector (weighted energy detector) performs well when the distribution is completely known. Therefore, it is important to consider the effect of uncertainty. For example, suppose that all we knew was that there is only a 1% chance that the satellite shadowing is small (say 5 dB) while the TV signal is severely shadowed (say greater than 30 dB). How would the weighted energy detector perform with this limited information?

**Theorem 14:** Let  $P_1$  be the received primary power at the secondary radio, and  $S_2$  denote the shadowing in the satellite

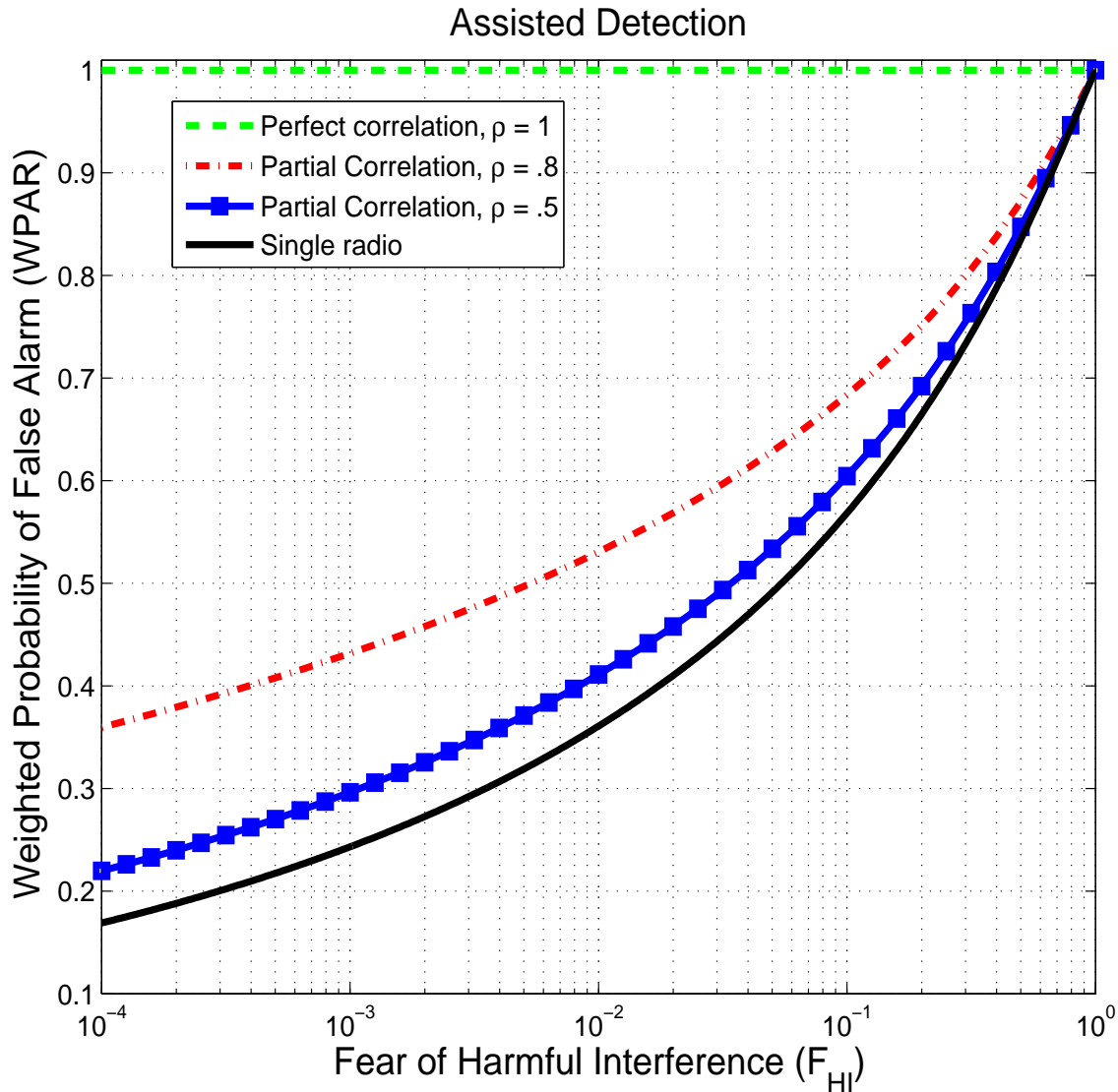


Fig. 16. Performance of a satellite-band assisted receiver versus that of a single radio with no assistance. The variance of satellite band fading was half the variance of the TV fading and complete model knowledge.

band to the secondary radio. Assume that the nominal distribution for  $(P_1, S_2)$  is

$$\begin{bmatrix} P_1 \\ S_2 \end{bmatrix} \sim \mathcal{N} \left( \begin{bmatrix} \mu(r) \\ \mu_2 \end{bmatrix}, \begin{bmatrix} \sigma_1^2 & -\rho \sigma_1 \sigma_2 \\ -\rho \sigma_1 \sigma_2 & \sigma_2^2 \end{bmatrix} \right), \quad (92)$$

where  $\mu(r)$  is a known monotonically decreasing function of the distance from the primary transmitter  $r$ , and  $(\rho, \mu_2, \sigma_1, \sigma_2)$  are known constants.

Fix  $0 \leq \beta_1, \beta_2 \leq 1$ . Assume that the set of uncertain distributions  $\mathbb{F}_r$  for  $(P_1, S_2)$  satisfies

- The marginals satisfy the respective individual quantile constraints, i.e.,  $\mathcal{P}(P_1 < \gamma(r, \beta_1)) = \beta_1$  and  $\mathcal{P}(S_2 < \gamma(\beta_2)) = \beta_2$ .
- The joint distribution satisfies  $\mathcal{P}(P_1 < \gamma(r, \beta_1), S_2 < \gamma(\beta_2)) = \beta_{12}$ .

Here, the constants  $\gamma(r, \beta_1)$ ,  $\gamma(\beta_2)$  and  $\beta_{12}$  are chosen such that the nominal distribution in (92) lies in the uncertain set  $\mathbb{F}_r$ .

That is,  $\gamma(r, \beta_1) = \sigma_1 \mathcal{Q}^{-1}(1 - \beta_1) + \mu(r)$ ,  $\gamma(\beta_2) = \sigma_2 \mathcal{Q}^{-1}(1 - \beta_2) + \mu_2$ , and,

$$\beta_{12} = \int_{-\infty}^{\gamma(r, \beta_1)} \int_{-\infty}^{\gamma(\beta_2)} \frac{1}{2\pi\sigma_1\sigma_2\sqrt{1-\rho^2}} \exp\left(-\frac{1}{2}[P_1 - \mu(r) S_2 - \mu_2] \begin{bmatrix} \sigma_1^2 & -\rho\sigma_1\sigma_2 \\ -\rho\sigma_1\sigma_2 & \sigma_2^2 \end{bmatrix}^{-1} [P_1 - \mu(r) S_2 - \mu_2]^T\right) dP_1 dS_2. \quad (93)$$

Now, consider the weighted-average detector in (86). The optimal detection threshold for this weighted-average detector is  $\lambda^* = \gamma(r_n, \beta_1) + \rho \frac{\sigma_1}{\sigma_2} \gamma(\beta_2)$ . Then, the safety/performance of the weighted-average detector is given by

$$F_{HI}(\beta_1, \beta_2, \beta_{12}) = \beta_1 + \beta_2 - \beta_{12}, \quad (94)$$

$$P_{FH}(r) = 1 - Q\left(\frac{\lambda^* - (\mu(r) + \rho \frac{\sigma_1}{\sigma_2} \mu_2)}{\sigma_1 \sqrt{1 - \rho^2}}\right). \quad (95)$$

*Proof:*  $F_{HI}$  can be written as:

$$\begin{aligned} F_{HI}(\beta_1, \beta_2, \beta_{12}) &= \sup_{F_r \in \mathbb{F}_r} \sup_{0 \leq r \leq r_n} \mathcal{P}(P_1 + \rho \frac{\sigma_1}{\sigma_2} S_2 < \lambda) \\ &\stackrel{(a)}{=} \sup_{F_r \in \mathbb{F}_{r_n}} \mathcal{P}(P_1 + \rho \frac{\sigma_1}{\sigma_2} S_2 < \lambda) \\ &\stackrel{(b)}{=} \beta_1 + \beta_2 - \beta_{12}. \end{aligned}$$

Here (a) is true because the worst-case distribution occurs at  $r_n$ . Equation (b) can be best understood by considering Figure 11 even though the quantiles  $\beta_1, \beta_2$  will probably be different for satellite-assisted detection. The weighted-average detector is  $P_1 + \rho \frac{\sigma_1}{\sigma_2} S_2$  which is similar to the diagonal blue line detector in Figure 11, but with a slope that depends on the correlation and relative magnitudes of the fading variances. For the satellite-assisted detector, the probability of region I is  $1 - (\beta_1 + \beta_2 - \beta_{12})$ . For  $\lambda > \gamma(r, \beta_1) + \rho \frac{\sigma_1}{\sigma_2} \gamma(\beta_2)$ , all four regions (I-IV) will contribute to  $F_{HI}$  and hence  $F_{HI}$  will be 1. For  $\lambda \leq \gamma(r, \beta_1) + \rho \frac{\sigma_1}{\sigma_2} \gamma(\beta_2)$  only regions II, III and IV contribute to  $F_{HI}$  and hence the value of  $F_{HI}$  is  $\beta_1 + \beta_2 - \beta_{12}$ . Since  $WPAR$  increases with  $\lambda$ , the optimal value of  $\lambda$  which keeps  $F_{HI}$  at  $\beta_1 + \beta_2 - \beta_{12}$  is  $\lambda^* = \gamma(r_n, \beta_1) + \rho \frac{\sigma_1}{\sigma_2} \gamma(\beta_2)$ . This means that,

$$F_{HI}(\beta_1, \beta_2, \beta_{12}) = 1 - \mathcal{P}(P_1 \geq \gamma(r_n, \beta_1) S_2 \geq \gamma(\beta_2)) = \beta_1 + \beta_2 - \beta_{12}. \quad (96)$$

Using the optimal  $\lambda^*$ , and the nominal model to compute the  $WPAR$ , we get

$$\begin{aligned} P_{FH}(r) &= \mathcal{P}_{F_r}(T(P_1, S_2) < \lambda^* | r_{actual} = r) \\ &= 1 - Q\left(\frac{\lambda^* - (\mu(r) + \rho \frac{\sigma_1}{\sigma_2} \mu_2)}{\sigma_1 \sqrt{1 - \rho^2}}\right). \end{aligned} \quad (97)$$

■

The achievable region of  $(F_{HI}, WPAR)$  is the convex hull of all the points generated by changing the values of  $\beta_1$  and  $\beta_2$ . This region is shown in Figure 17. The performance is significantly worse than the performance when the channel model is completely trusted. The main reason for the poor performance is that three quadrants  $[\mathcal{P}(\{P_1 < \gamma(r, \beta_1)\} \cup \{S_2 < \gamma(\beta_2)\})]$

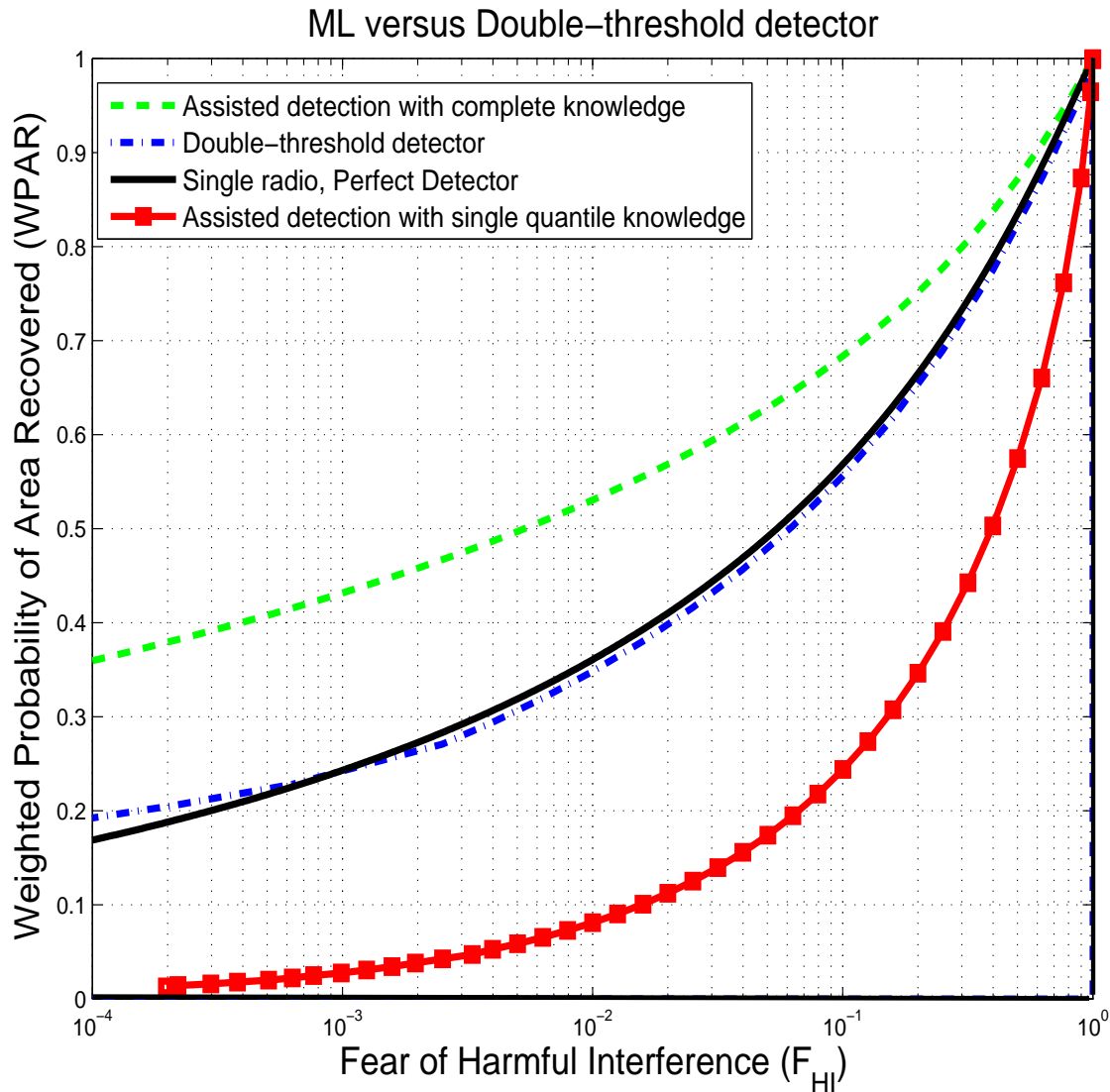


Fig. 17. Performance of the double-threshold detector as compared to an ML detector. If the channel model is uncertain, the double-threshold detector is preferred.

contribute to the  $F_{HI}$  for the weighted-average detector.

The counterpart to the OR-rule here is the double-threshold detector. This detector declares that the primary is absent only if  $P_1 < \gamma(r_n, \beta_1)$  and  $S_2 < \gamma(\beta_2)$  i.e. when the primary signal is low enough and the satellite signal is not significantly faded. In this case the fear of harmful interference is  $\beta_{12}$ , which is lesser than the fear of harmful interference,  $\beta_1 + \beta_2 - \beta_{12}$ , for the weighted-average detector. The performance of this detector is compared to the weighted-average detector in Figure 17. This shows that if the information about the channel model is limited, the double-threshold detector is preferred. In fact, the double-threshold rule with limited knowledge can outperform even a single-radio detector with complete knowledge. This shows that additional information about the shadowing environment is useful even if it is only binary information (i.e. whether we are indoors (deeply shadowed) or outdoors).

## VII. CONCLUSIONS

Static frequency planning results in bands being allocated to homogeneous services over large spatial areas and for long times in order to isolate and thus protect the robust operation of heterogeneous wireless systems while preserving their individual freedom. This results in significant underutilization of the spectrum from the perspective of users that could operate on much smaller space-time scales and thereby fit within the “spectrum holes” left by the static allocations. Dynamic spectrum access can allow the utilization of these spectrum holes.

To do this, strategies for sensing spectrum holes must satisfy two objectives. The first is safety — the primary users must be guaranteed that they will not experience undue interference. The second is efficiency — as much of the spectrum hole as possible must be reclaimed. The core problem is that the incentives of those proposing and implementing the sensing strategy are aligned with the second objective, but not the first. As a result, the primary users have no rational reason to trust the secondary users’ assurances and this results in asymmetric uncertainty.

To reflect this tension and to allow a unified treatment of spectrum sensing, this paper has introduced two distinct metrics. To guarantee safety, the “Fear of Harmful Interference”  $F_{HI}$  from the detector must be kept low enough no matter which radio deployment and environmental model turns out to be true. It is only the primary user’s uncertainty set that matters here. Consensus between the regulators, primary users, and secondary users has to be achieved regarding this uncertainty and so it is likely to remain large. Every sensing strategy will have its own critical uncertainties that must be bounded.

In this paper, quantile models have been proposed for uncertain probability distributions (e.g. for shadowing) while secondary radio positions have been considered unconstrained. In multiuser settings, the degree of shadowing correlation turns out to be a very significant uncertainty. It has been suggested that it might be easier to achieve a firm consensus regarding the correlation of shadowing across different frequencies for a single radio than it is to achieve a consensus regarding the shadowing correlation across users. This remains to be explored more fully, but the  $F_{HI}$  metric seems to be the right way to capture the otherwise vague notion of safety while still allowing significant innovation at the detector level.

For performance purposes, the secondary user has no reason to lie and is free to analyze its own performance using any desired probability model and utility function. The core issue here is one of simplicity and generalizability. To enable high-level comparisons between detection strategies, it is important to be able to decouple the interaction among different primary users while capturing the key effects. Restricting attention to spectrum holes that are very long lived in time, we have argued that the high-order terms are:

- As we get further away from any primary transmitter, there is an increasing chance that we will be within the service footprint of another primary transmitter.
- Area closer to the primary user’s footprint is more valuable (in a business or utility sense) than area far away because primary users are likely to have positioned their transmitters so as to serve a maximal number of humans.

Therefore, the proposed “Weighted Probability of Area Recovered” (WPAR) metric uses a discounting-function to weigh the probability of recovering area at a given distance away from a single primary transmitter. While exponential discounting has been used here for convenience, it remains an interesting open question to determine what the right discounting functions are for different application scenarios.

By using these metrics, this paper has shown that the popularly used metrics of sensitivity,  $P_{FA}$ , and  $P_{MD}$  (such as the  $-116$  dBm rule used by the IEEE 802.22 process) are overly constraining. Even an ideal detector (one with  $P_{FA} = P_{MD} = 0$  for a desired sensitivity) has poor WPAR performance when facing uncertain fading. Too much valuable area must be sacrificed to achieve the desired robustness — effectively turning this into a static guard band by another name. However, the  $F_{HI}$  and WPAR metrics allow the principled consideration of alternative strategies such as multiuser cooperation and show exactly which uncertainties must be resolved (and to what resolution) in order to be able to guarantee both safety and high performance for a detector of a given complexity. Therefore, we suggest that specifications for detection strategies be expressed at the  $F_{HI}$  and WPAR level rather than in terms of a desired sensitivity and ROC.

This paper represents the beginning of a story rather than the end of one. Much remains to be done. In particular:

- Cooperative sensing strategies that utilize assisted detection need to be analyzed. The performance of such strategies under our new  $F_{HI}$  and  $WPAR$  metrics needs to be evaluated [89].
- The tradeoffs between the time-overhead (sensing time + cooperative message exchange) and the space-overhead (WPAR effects + sensing-MAC effects [90]) need to be understood. It is here that different signal-processing strategies are likely to distinguish themselves. Such a space-time hole is illustrated in Figure 18 where the combination of temporal and spatial margins/overheads is illustrated.
- Under the traditional metric of sensitivity, an SNR wall for a sensing algorithm sets a bound on how sensitive a detector can be given the uncertain model for the noise process [16]. The role of SNR walls must also be understood in the context of WPAR and  $F_{HI}$  since sensitivity is now implicit rather than explicit.
- The simple quantile models that have been proposed here are intuitively clear and easy to use but clearly do not represent the form of uncertainty representation that is both unambiguously verifiable and realistic. The example of the subtle role of constructive interference in Section V-C made that clear. Since consensus is required between primary and secondary users, one would prefer an uncertainty model that came with an experimental certificate of correctness.
- The  $F_{HI}$  metric currently captures only one dimension of fear — that of optimistic assumptions regarding the environment. In practice, there is also the fear of dishonest implementations.<sup>20</sup> The regulators, primary users, and secondary users should only need to achieve consensus regarding some key features of the wireless system implementation rather than for every aspect.<sup>21</sup> The safety of the rest of the implementation should rely on self-regulation (or peer regulation) through the design of an appropriately lightweight enforcement mechanism.

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<sup>20</sup>Even after we agree to the rules of a game, we still need a way to make sure that players adhere to those rules.

<sup>21</sup>Some might wonder “why can't we all just get along?” It is important to remember that there are business reasons why primary users might wish to hinder secondary use so as to forestall competition [91]. Thus it is preferable to have only a few such regulatory hurdles.



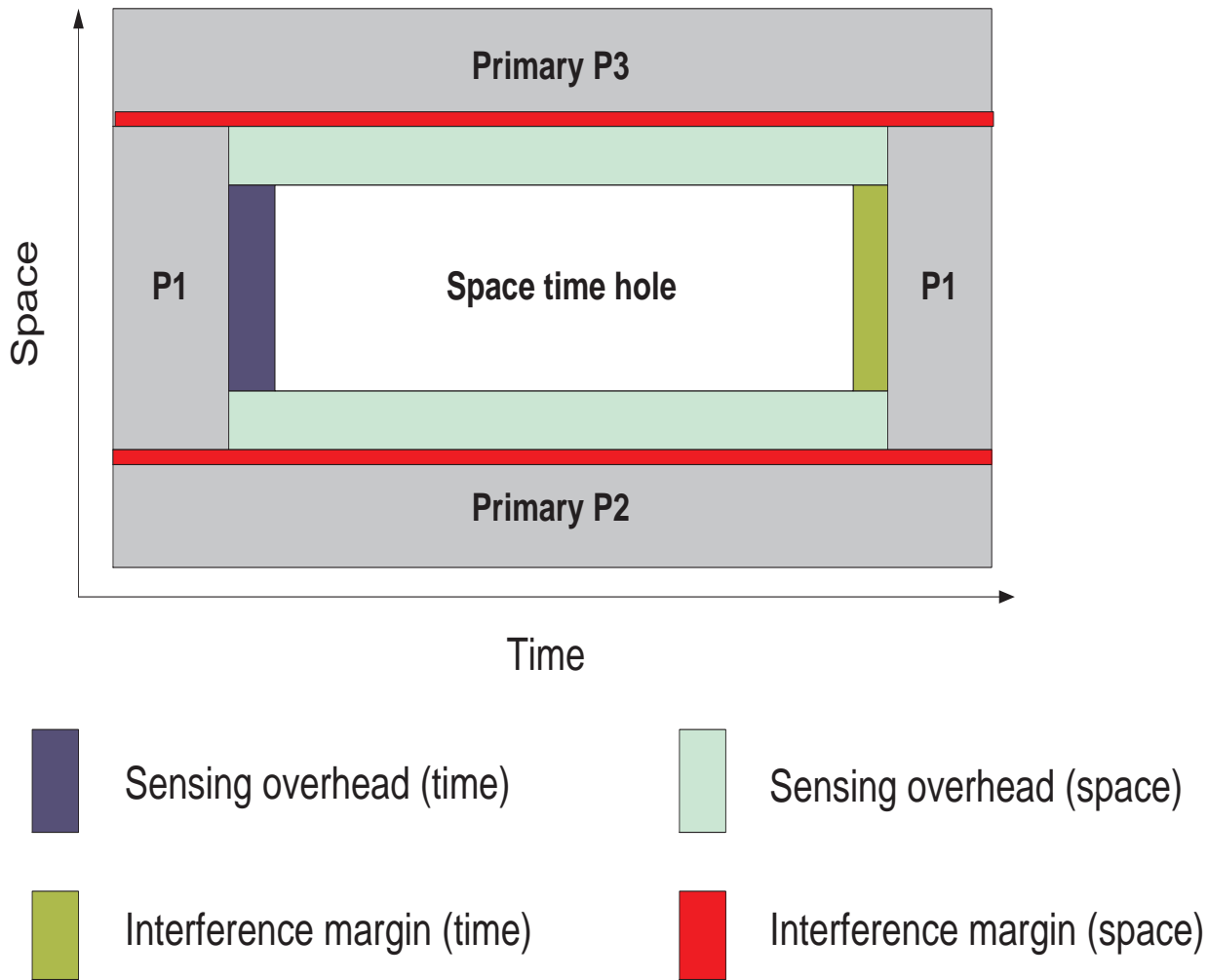


Fig. 18. A space-time hole. Primary users  $P_1$ ,  $P_2$  and  $P_3$  occupy different space-time regions but the same frequency band. The secondary user can recover the hole when  $P_1$  ceases transmission albeit with some time lost due to temporal sensing overhead. When  $P_1$  reappears, the secondary user can still transmit for a finite duration (temporal interference margin). Corresponding spatial interference margins and sensing overheads are also shown in the figure.

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